## ACCESS MANAGEMENT EXCEPTION REQUEST: AM-E <br> ACCESS MANAGEMENT REGULATIONS 24 VAC 30-73 <br> SECTION 120

| Submitted by: Andy Sadler - Doswell Ventures, LLC |  | Date: $10-08-2018$ |
| :--- | :--- | :--- |
| Email Address: asadler@askwoodfin.com | Phone: (804) 730-4500 |  |
| Address: 3800 Patterson Avenue, Richmond, VA 23221 | Rte \# U.S. 60 | Locality: York Co. / James City Co. |
| Project Name: Lightfoot Road C-Store |  |  |
| Description of Project: <br> Proposed convenience store with 12 fueling positions (f.p.) to replace the existing 10 f.p. Exxon station located in the <br> northwest quadrant of the U.S. 60 Richmond Road at Lightfoot Road intersection. The proposed access plan includes closing <br> the eastern right-in / right-out driveway on U.S. 60, and shifting the site driveway on Lightfoot Road approximately 180 feet to <br> the north, and converting it to a partial access driveway with a right-in / right-out / left-out configuration. |  |  |
| VDOT District: Hampton Roads | Area Land Use Engineer: Glenn Brooks, P.E. |  |

## NOTES:

(1). Submit this form and any attachments to one of the District's Area Land Use Engineers.
(2). See Section 120 of the Regulations for details on the requirements, exceptions, and exception request review process.
(3). Attach additional information as necessary to justify the exception request(s).
(4). If a traffic engineering study is required, the decision on the request will be based on VDOT engineering judgment.
(5). Use the LD-440 Design Exception or the LD-448 Design Waiver forms for design and engineering standards, e.g. radius, grade, sight distance. See IIM-LD-227 on VDOT web site for additional instructions.

## Select the Exception(s) Being Requested

Exception to the shared commercial entrance requirement. (Access M. Regulations Section 120 C.2) Reason for exception:
$\square$ A. An agreement to share the entrance could not be reached with adjoining property owner.
Attached: Written evidence that adjoining property owner will not share the entrance.B. Physical constraints: topography, adjacent hazardous land use, stream, wetland, other.
$\square$ Specify constraint:

Attached: Documentation of constraint such as aerial photo or topographic map.
Exception to the vehicular connection to adjoining undeveloped property requirement. (Section 120 C.4) Reason for exception:
$\square$ A. Physical constraints: topography, adjacent hazardous land use, stream, wetland, other.
$\square$ Specify constraint:
$\square$ Attached: Documentation of constraint such as aerial photo or topographic map.B. Other reason:

Exception to the commercial entrance shall not be located within the functional area of an intersection requirement. (See Regulation Section 120 C. 1; Appendix F, Rd Design Manual)

Attached: A traffic engineering study documenting that the operation of the intersection and public safety will not be adversely impacted.

## EXCEPTION TO THE SPACING STANDARDS FOR:

- Commercial entrances; intersections/median crossovers (Table 2-2);
- Commercial entrances/intersections near interchange ramps (Tables 2-3, 2-4); or
- Corner clearance (Figure 4-4). Appendix F, Road Design Manual

Information on the Exception Request

## ON A STATE HIGHWAY

Functional classification: Principal Arterial: $\square$ Minor Arterial: $\square \quad$ Collector: $\square$ Local: $\square$ Posted speed limit: _ 45 mphNEAR AN INTERCHANGE RAMP (Submittal of a traffic engineering study required)
$\square$ CORNER CLEARANCE (Submittal of a traffic engineering study required)
Type of intersection/entrance: Signalized $\square$ Unsignalized $\square$ Full Access $\square$ Partial Access $\square$ Required spacing distance_ 305 _ft

Proposed spacing distance $\qquad$ ft 280 ft to east / 120 feet to west along U.S. 60

Requested exception: Reduction in required spacing $\qquad$ ft 25 ft to east / 185 feet to west along U.S. 60

## REASON FOR EXCEPTION:

A. To be located on an older, established business corridor along a highway where existing spacing did not meet the standards prior to 7/1/08 or 10/14/09. (Regulation Section 120 C.3.c)$\checkmark$ Attached: Dated aerial photo of corridor identifying proposed entrance/intersection location.
B. Not enough property frontage to meet spacing standard, but the applicant does not want a partial access right-in/right-out entrance. (Section 120 C.3.f)

Attached: A traffic engineering study documenting that left turn movements at the entrance will not have a negative impact on highway operation or safety.
C. To be located within a new urbanism mixed use type development. (Section 120 c.3.d)
$\square$ Attached: The design of the development and compliance with intersection sight distance.D. The proposed entrance meets the signal warrants but does not meet the signalized intersection spacing standard. The applicant requests an exception to the spacing standard.

Attached: A traffic engineering study that (i) evaluates the location's suitability for a roundabout and (ii) provides documentation that the proposed signal will not impact safety and traffic flow. (Section 120 C.5)E. The development's $2^{\text {nd }}$ (or additional) entrance does not meet the spacing standards but is necessary for the streets to be accepted into the secondary system. (Section 120 C.3.e)
Attached: Information on the development that identifies the location of entrances.F. To be located within the limits of a VDOT and locality approved access management corridor plan.

Attached: Aerial photo of corridor identifying proposed entrance/intersection location. (Sect 120 C.3.b)

## FOR VDOT USE ONLY

| Recommendation on Exception Request: Approve | $\square$ | Deny |  |
| :--- | :--- | :--- | :--- |
|  | Date: |  |  |
| Area Land Use Engineer or: |  |  |  |

Remarks:

| Exception Request Action: Approved $\square$ | Denied $\square$ | Date: |
| :--- | :--- | :--- |
| District Administrator or Designee: |  |  |
| Name (and position if Designee) |  |  |
| Remarks: |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |

October 8, 2018

Ms. Susan Kassel
Director of Planning and Development Services
York County
224 Ballard Street
Yorktown, Virginia 23690
Phone: (757) 890-3531
Reference: Lightfoot Road C-Store
Traffic Impact Analysis (TIA) and Access Management Exception (AME) Request
York County and James City County, Virginia
Dear Ms. Kassel,
There is currently an Exxon station with 10 fueling positions in the northwest quadrant of the U.S. 60 (Richmond Road) at Lightfoot Road intersection. The Exxon station has two right-in / right-out driveways on U.S. 60, and one full-movement driveway on Lightfoot Road. The applicant is planning to redevelop the site, and construct a new convenience store with 12 fueling positions, and Ramey Kemp \& Associates, Inc. (RKA) has performed this TIA to support the proposed redevelopment.

Based on meetings and coordination with the Virginia Department of Transportation (VDOT), the proposed access plan includes closing the eastern right-in / right-out driveway on U.S. 60, and shifting the site driveway on Lightfoot Road approximately 180 feet to the north, converting it to a partial access driveway with a right-in / right-out / left-out configuration, and constructing a southbound right-turn taper on Lightfoot Road. If approved, the proposed C-store is expected to be built in 2020. Figure 1 shows the site location and study intersections, and Figure 2 shows the conceptual site plan.

Based on the TIA scoping meeting with you and VDOT on February 6, the purpose of this letter report is to provide the following:

- Trip generation calculations
- Capacity analysis of the study intersections
- Evaluation of turn lane warrants at the site driveways
- AME Request for the existing right-in / right-out driveway on U.S. 60 that will remain


## Existing Roadway Conditions

U.S. 60 (Richmond Road) is a Principal Arterial with an average daily traffic (ADT) volume of approximately 20,000 vehicles per day ( vpd ), and a posted speed limit of 45 miles per hour ( mph ) in the vicinity of the site.

Lightfoot Road is a Major Collector with an ADT volume of approximately 8,800 vpd, and a posted speed limit of 45 mph in the vicinity of the site.

Figure 3 shows the existing lane configuration.

## Existing Traffic Volumes

The AM peak hour (7:00 to 9:00 AM) and PM peak hour (4:00 to 6:00 PM) turning movement counts were conducted by VHB Engineering at the following intersection in October 2016:

- U.S. 60 at Lightfoot Road / Williamsburg Outlet Mall Driveway

Based on discussion with VDOT, these traffic volumes were grown by $1.0 \%$ per year for two years to estimate the existing 2018 traffic volumes.

The AM peak hour (7:00 to 9:00 AM) and PM peak hour (4:00 to 6:00 PM) turning movement counts were conducted by Peggy Malone \& Associates at the following intersections on June 12, 2018:

- U.S. 60 at West Right-in / Right-out Driveway
- U.S. 60 at East Right-in / Right-out Driveway
- Lightfoot Road at Full-Movement Driveway

The traffic count data are enclosed, and the existing 2018 volumes are shown in Figure 4.

## Approved Development

Lightfoot Apartments is a potential mixed-use development located in the southeast quadrant of the Lightfoot Road at Old Mooretown Road intersection. The site plan includes 216 apartments, 32 townhomes, up to 13,000 square feet (s.f.) of general office and retail space, and up to 7,000 s.f. of restaurant space. The Lightfoot Apartment site trips shown in Figure 5 are based on the September 2017 Lightfoot Apartments TIA prepared by VHB.

Lightfoot Marketplace is a commercial center on the south side of U.S. 60 across from the site. The original TIA was performed by Bryant B. Goodloe, P.C. in October 2013, which included a number of outparcels along U.S. 60, which are now approved for construction:

- 26,625 s.f. of medical / dental office space
- 33,943 s.f. of general retail space
- 5,000 s.f. expansion of the existing Harris Teeter store
- Panera restaurant with 100 seats
- Fuel center with 10 fueling positions

Bryant B. Goodloe, P.C. submitted an updated trip generation memo for these uses in September 2017. The trip generation potential and distribution of those trips are included in this analysis based on that memo.

Ms. Susan Kassel
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The trip generation potential of the Lightfoot Marketplace outparcels during a typical weekday, AM peak hour, and PM peak hour was estimated using the methodologies published by the Institute of Transportation Engineers (ITE) Trip Generation Manual - $10^{\text {th }}$ Edition. Table 1 summarizes the trip generation calculations for the Lightfoot Marketplace outparcels.

Table 1
Lightfoot Marketplace Outparcels - ITE Trip Generation - Weekday - $\mathbf{1 0}^{\text {th }}$ Edition

| Land Use(ITE Land Use Code) | Size | Average Daily Traffic (vpd) |  | AM Peak Hour (vph) |  | PM Peak Hour (vph) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Enter | Exit | Enter | Exit | Enter | Exit |
| Medical-Dental Office (720) | 26,625 s.f. | 468 | 468 | 58 | 16 | 26 | 66 |
| General Retail Space (820) | 33,943 s.f. | 1,442 | 1,442 | 20 | 12 | 117 | 127 |
| Supermarket (850) | $5,000 \text { s.f. }$ <br> expansion | 784 | 784 | 11 | 8 | 42 | 41 |
| Fast-Food Restaurant with Drive-Thru Window (934) | 100 seats | 976 | 976 | 69 | 62 | 51 | 46 |
| Gasoline / Service Station (944) | 10 f.p. | 860 | 860 | 51 | 52 | 70 | 70 |
| Driveway Volumes |  | 4,530 | 4,530 | 209 | 150 | 306 | 350 |
| Pass-By Trips General Retail - Supermarket - 36 Fast-Food Restaurant $-49 \%$ Gas Station $-58 \%$ AM | $\begin{aligned} & \text { M / } 50 \% \text { PM } \\ & 2 \% \mathrm{PM} \\ & \hline \end{aligned}$ | $\begin{aligned} & -490 \\ & -282 \\ & -483 \\ & -430 \\ & \hline \end{aligned}$ | $\begin{aligned} & -490 \\ & -282 \\ & -483 \\ & -430 \\ & \hline \end{aligned}$ | $\begin{array}{r} -5 \\ -3 \\ -32 \\ -29 \\ \hline \end{array}$ | $\begin{gathered} -5 \\ -3 \\ -32 \\ -29 \\ \hline \end{gathered}$ | $\begin{aligned} & -41 \\ & -14 \\ & -24 \\ & -29 \\ & \hline \end{aligned}$ | $\begin{aligned} & -41 \\ & -14 \\ & -24 \\ & -29 \\ & \hline \end{aligned}$ |
| Net New External Trips |  | 2,845 | 2,845 | 137 | 81 | 198 | 242 |

The Lightfoot Marketplace trip distributions and assignments are shown in Figure 6. The total approved development trips are shown in Figure 7.

## Background Traffic Growth

Based on discussion with you and VDOT, the 2018 peak hour traffic volumes were grown by an annual rate of $1.0 \%$ for two years to estimate the 2020 peak hour traffic volumes. The no-build 2020 peak hour trips were estimated by growing the existing volumes for two years and combining the approved development trips (Figure 7). Figure 8 shows the estimated 2020 no-build peak hour traffic volumes.

## Trip Generation

The trip generation potential of the proposed C-store during a typical weekday, AM peak hour, and PM peak hour was estimated using the methodologies published by the ITE Trip Generation Manual - $10^{\text {th }}$ Edition. Table 2 summarizes the trip generation calculations.

Table 2
Lightfoot Road C-Store - ITE Trip Generation - Weekday - 10 ${ }^{\text {th }}$ Edition

| Land Use <br> (ITE Land Use Code) | Size | Weekday <br> Daily Traffic <br> (vpd) |  | AM Peak Hour <br> (vph) |  | PM Peak Hour <br> (vph) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Exit | Enter | Exit | Enter | Exit |  |
| Super Convenience Market / <br> Gas Station (960) | 12 f.p. | 1,383 | 1,383 | 169 | 169 | 138 | 138 |
| Pass-By Trips - 63\% AM / 66\% PM |  | -892 | -892 | -106 | -106 | -91 | -91 |
| Net New External Trips |  | $\mathbf{4 9 1}$ | $\mathbf{4 9 1}$ | $\mathbf{6 3}$ | $\mathbf{6 3}$ | $\mathbf{4 7}$ | $\mathbf{4 7}$ |

C-stores attract pass-by trips, which are made by drivers who are already driving by the site today and will visit the C-store in the future because it is convenient. Table 2 shows the ITE pass-by trip adjustments that were applied in the study.

## Site Traffic Distribution

The following primary traffic distribution was applied based on a review of the existing traffic volumes, the adjacent roadway network, and engineering judgement:

- $40 \%$ to / from the east on U.S. 60
- $30 \%$ to / from the west on U.S. 60
- $25 \%$ to / from the north on Lightfoot Road
- $5 \%$ to / from the south on the Williamsburg Outlet Mall Driveway

It was assumed that all of the pass-by trips will originate from U.S. 60, and the following pass-by trip directional distributions were used:

- $75 \%$ westbound / $25 \%$ eastbound

Figure 10 shows the primary and pass-by site trip distributions, Figure 11 shows the primary and pass-by site trip assignments, and Figure 12 shows the total site trips.

## Existing Exxon Trip Adjustment

Under build conditions, the existing Exxon trips were removed from the roadway network as shown in Figure 9. The build 2020 peak hour volumes, which are shown in Figure 12, were estimated by combining the no-build volumes (Figure 8) with the existing trip adjustment (Figure 9) and the total site trips (Figure 12).

Ms. Susan Kassel
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## VDOT Intersection Spacing Standards

VDOT requires at least 250 feet of separation between partial access driveways and full-movement intersections on Major Collector roadways posted 45 mph . The proposed right-in / right-out / left-out driveway on Lightfooot Road is approximately 380 feet north of the intersection of U.S. 60 and Lightfoot Road, which exceeds VDOT's minimum intersection spacing standards.

VDOT requires at least 305 feet of separation between partial access driveways and full-movement driveways on Principal Arterial roadways posted 45 mph . The proposed right-in / right-out driveway on U.S. 60 is approximately 280 feet west of Lightfoot Road and approximately 120 east of the Hardee's driveway, which does not meet VDOT's minimum intersection spacing standards. An Access Management Exception (AME) request form is enclosed.

## VDOT Turn Lane Warrant Analysis

The projected build-out AM and PM peak hour traffic volumes at the proposed site driveway on Lightfoot Road were compared to the turn lane warrants in the Virginia Department of Transportation (VDOT) Access Management Design Standards for Entrances and Intersections.

- A southbound right-turn lane or taper on Lightfoot Road is not warranted, but the applicant is proposing a southbound right-turn taper to improve Lightfoot Road as much as possible along the property frontage

The VDOT turn lane warrant diagram is enclosed for reference.

## Traffic Capacity Analysis

Traffic capacity analysis for the study intersections was performed using Synchro 10, which is a comprehensive software package that allows the user to model signalized and unsignalized intersections to determine levels-ofservice based on the thresholds specified in the Highway Capacity Manual (HCM) - $6^{\text {th }}$ Edition.

Table 3 summarizes the capacity analysis results for the signalized intersection of U.S. 60 at Lightfoot Road / Williamsburg Outlet Mall Driveway.

Table 3
Level-of-Service Summary for U.S. 60 at Lightfoot Road / Williamsburg Outlet Mall Driveway

| CONDITION | $\begin{aligned} & \text { LANE } \\ & \text { GROUP } \end{aligned}$ | AM PEAK HOUR |  |  |  | PM PEAK HOUR |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { Lane } \\ & \text { LOS } \end{aligned}$ | Lane Delay (sec) | Queue <br> (ft) | $\begin{aligned} & \hline \text { Overall } \\ & \text { LOS } \\ & \text { (Delay) } \end{aligned}$ | $\begin{aligned} & \text { Lane } \\ & \text { LOS } \end{aligned}$ | Lane Delay (sec) | Queue <br> (ft) | $\begin{gathered} \text { Overall } \\ \text { LOS (Delay) } \end{gathered}$ |
| Existing 2018 <br> Traffic Conditions | EBU/L | D | 50.1 | 219 |  | E | 71.4 | 320 |  |
|  | EBT | B | 15.8 | 218 |  | C | 25.7 | 365 |  |
|  | EBR | A | 0.1 | 0 |  | A | 0.2 | 0 |  |
|  | WBL | D | 49.1 | 45 |  | D | 50.6 | 85 |  |
|  | WBT | C | 25.1 | 207 |  | C | 32.1 | 378 |  |
|  | WBR | A | 0.1 | 0 |  | A | 0.2 | 0 |  |
|  | NBL | D | 49.4 | 51 | $(23.6 \mathrm{sec})$ | D | 50.7 | 85 | $(30.7 \mathrm{sec})$ |
|  | NBL/T | D | 49.4 | 53 |  | D | 50.5 | 87 |  |
|  | NBR | A | 1.2 | 0 |  | A | 1.7 | 0 |  |
|  | SBT/L | D | 50.7 | 173 |  | E | 57.8 | 371 |  |
|  | SBR | A | 8.9 | 49 |  | A | 7.8 | 78 |  |
| No-Build 2020 <br> Traffic Conditions | EBU/L | D | 50.8 | 212 |  | E | 75.3 | 319 |  |
|  | EBT | C | 20.3 | 214 |  | C | 32.1 | 356 |  |
|  | EBR | A | 4.0 | 34 |  | A | 4.6 | 47 |  |
|  | WBL | D | 53.4 | 104 |  | E | 58.5 | 174 |  |
|  | WBT | C | 27.9 | 218 |  | D | 35.9 | 382 |  |
|  | WBR | A | 0.1 | 0 |  | A | 0.2 | 0 |  |
|  | NBL | D | 51.3 | 76 | $(26.0 \mathrm{sec})$ | D | 54.2 | 140 | (35.1 sec) |
|  | NBL/T | D | 51.0 | 76 |  | D | 54.1 | 141 |  |
|  | NBR | A | 2.2 | 0 |  | B | 11.6 | 60 |  |
|  | SBT/L | D | 51.7 | 195 |  | E | 65.4 | 396 |  |
|  | SBR | A | 8.6 | 52 |  | B | 13.8 | 138 |  |
| Build 2020 <br> Traffic Conditions | EBU/L | D | 51.7 | 251 |  | E | 60.6 | 315 |  |
|  | EBT | C | 20.7 | 201 |  | C | 33.5 | 350 |  |
|  | EBR | A | 3.9 | 34 |  | A | 4.7 | 47 |  |
|  | WBL | E | 57.1 | 107 |  | E | 56.2 | 172 |  |
|  | WBT | C | 32.0 | 229 |  | D | 48.0 | 458 |  |
|  | WBR | A | 0.1 | 0 |  | A | 0.2 | 0 |  |
|  | NBL | D | 52.2 | 77 | $(28.3 \mathrm{sec})$ | D | 54.4 | 140 | $(39.0 \mathrm{sec})$ |
|  | NBL/T | D | 52.3 | 81 |  | D | 54.3 | 143 |  |
|  | NBR | A | 2.3 | 0 |  | B | 11.6 | 60 |  |
|  | SBT/L | D | 52.2 | 239 |  | E | 72.7 | 470 |  |
|  | SBR | A | 7.7 | 51 |  | B | 16.4 | 163 |  |

Capacity analysis indicates this intersection currently operates at LOS C during the AM and PM peak hours. Under no-build 2020 traffic conditions, this intersection is expected to operate at LOS C during the AM peak hour and at LOS D during the PM peak hour. Under build 2020 traffic conditions, this intersection is projected to continue to operate at LOS C during the AM peak hour and at LOS D during the PM peak hour with all movements operating at LOS E or better.

Ms. Susan Kassel
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The following improvement is recommended to accommodate the projected queue length on the eastbound U.S. 60 left-turn lane:

- Extend the eastbound left-turn lane on U.S. 60 from 275 feet to 325 feet

Table 4 summarizes the capacity analysis results for the unsignalized intersection of Lightfoot Road at Site Driveway.

Table 4
Level-of-Service Summary for Lightfoot Road at Site Driveway

| CONDITION | $\begin{aligned} & \text { LANE } \\ & \text { GROUP } \end{aligned}$ | AM PEAK HOUR |  |  |  | PM PEAK HOUR |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { Lane } \\ & \text { LOS } \end{aligned}$ | Lane Delay (sec) | Queue <br> (ft) | $\begin{aligned} & \hline \text { Overall } \\ & \text { LOS } \\ & \text { (Delay) } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { Lane } \\ & \text { LOS } \end{aligned}$ | Lane Delay (sec) | Queue <br> (ft) | $\begin{gathered} \hline \text { Overall } \\ \text { LOS } \\ \text { (Delay) } \\ \hline \end{gathered}$ |
| Existing 2018 Traffic Conditions | $\begin{gathered} \text { EBL }^{1} \\ \text { EBR }^{1} \\ \text { NBL/T² } \\ \text { SBT/R } \end{gathered}$ | $\begin{aligned} & \text { B } \\ & \text { B } \\ & \text { A } \end{aligned}$ | $\begin{gathered} 14.3 \\ 10.1 \\ 8.0 \end{gathered}$ | $\begin{aligned} & 3 \\ & 0 \\ & 0 \\ & - \end{aligned}$ | $\mathrm{N} / \mathrm{A}^{3}$ | C <br> B <br> A | $\begin{gathered} 22.4 \\ 12.9 \\ 9.0 \end{gathered}$ | $\begin{aligned} & 3 \\ & 0 \\ & 0 \\ & - \end{aligned}$ | $\mathrm{N} / \mathrm{A}^{3}$ |
| No-Build 2020 Traffic Conditions | $\begin{gathered} \text { EBL }^{1} \\ \text { EBR }^{1} \\ \text { NBL/T² } \\ \text { SBT/R } \end{gathered}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~B} \\ & \mathrm{~A} \end{aligned}$ | $\begin{gathered} 15.1 \\ 10.5 \\ 8.1 \end{gathered}$ | $\begin{aligned} & 3 \\ & 0 \\ & 0 \end{aligned}$ | $\mathrm{N} / \mathrm{A}^{3}$ | C <br> B <br> A | $\begin{gathered} 24.3 \\ 13.3 \\ 9.1 \end{gathered}$ | $\begin{aligned} & 3 \\ & 0 \\ & 0 \\ & - \end{aligned}$ | $\mathrm{N} / \mathrm{A}^{3}$ |
| Build 2020 <br> Traffic Conditions | $\begin{gathered} \text { EBL }^{1} \\ \text { EBR }^{1} \\ \text { NBT } \\ \text { SBT/R } \end{gathered}$ | $\begin{aligned} & \text { C } \\ & \text { B } \end{aligned}$ | $\begin{aligned} & 15.4 \\ & 11.3 \end{aligned}$ | $\begin{gathered} 3 \\ 13 \end{gathered}$ | $\mathrm{N} / \mathrm{A}^{3}$ | D B | 25.5 14.8 - - | $\begin{gathered} 5 \\ 13 \end{gathered}$ | $\mathrm{N} / \mathrm{A}^{3}$ |

1. Level of service for minor approach.
2. Level of service for major street left turn movement.
3. HCM methodology does not provide lane group or overall LOS, delay, and queue lengths for major street through movements or right turns at unsignalized intersections.

Capacity analysis indicates the minor street left-turn movement currently operates with short delays (less than 25 seconds) during the AM and PM peak hours. Under no-build 2020 traffic conditions, the minor street leftturn movement is expected to continue to operate with short delays (less than 25 seconds) during the AM and PM peak hours.

The proposed redevelopment includes shifting this driveway approximately 180 feet to the north along Lightfoot Road, converting it to partial access with a right-in / right-out / left-out configuration, and constructing a southbound right-turn taper on Lightfoot Road. Under the build 2020 traffic conditions, the minor street left-turn movement is projected to operate with short delays (less than 25 seconds) during the AM peak hour, and with moderate delays (between 25 and 50 seconds) during the PM peak hour with the proposed improvements.

Table 5 summarizes the capacity analysis results for the unsignalized intersection of U.S. 60 at Right-in / Rightout Driveway.

Table 5
Level-of-Service Summary for U.S. 60 at Right-in / Right-out Driveway

| CONDITION | $\begin{gathered} \text { LANE } \\ \text { GROUP } \end{gathered}$ | AM PEAK HOUR |  |  |  | PM PEAK HOUR |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { Lane } \\ & \text { LOS } \end{aligned}$ | $\begin{gathered} \text { Lane } \\ \text { Delay } \\ \text { (sec) } \end{gathered}$ | Queue <br> (ft) | $\begin{aligned} & \hline \text { Overall } \\ & \text { LOS } \\ & \text { (Delay) } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { Lane } \\ & \text { LOS } \end{aligned}$ | $\begin{gathered} \hline \begin{array}{c} \text { Lane } \\ \text { Delay } \\ \text { (sec) } \end{array} \\ \hline \end{gathered}$ | Queue <br> (ft) | $\begin{gathered} \hline \text { Overall } \\ \text { LOS } \\ \text { (Delay) } \\ \hline \end{gathered}$ |
| Existing 2018 Traffic Conditions | EBT <br> WBT <br> WBR <br> SBR ${ }^{1}$ |  | $\begin{gathered} - \\ - \\ - \\ 10.8 \end{gathered}$ | $3$ | $\mathrm{N} / \mathrm{A}^{2}$ | B |  | $\overline{5}$ | $\mathrm{N} / \mathrm{A}^{2}$ |
| No-Build 2020 Traffic Conditions | EBT <br> WBT <br> WBR <br> SBR $^{1}$ | - | $11.1$ | $3$ | $\mathrm{N} / \mathrm{A}^{2}$ | - | $15.7$ | $5$ | $\mathrm{N} / \mathrm{A}^{2}$ |
| Build 2020 <br> Traffic Conditions | EBT <br> WBT <br> WBR <br> $\mathrm{SBR}^{1}$ | - | $11.4$ | $10$ | $\mathrm{N} / \mathrm{A}^{2}$ | - | - - - 16.7 | $15$ | $\mathrm{N} / \mathrm{A}^{2}$ |

1. Level of service for minor approach.
2. HCM methodology does not provide lane group or overall LOS, delay, and queue lengths for major street through movements or right turns at unsignalized intersections.

Capacity analysis indicates the minor street right-turn movement currently operates with short delays (less than 25 seconds) during the AM and PM peak hours. Under no-build and build 2020 conditions, the minor street right-turn movement is expected to continue to operate with short delays (less than 25 seconds) at build out of the proposed redevelopment. No improvements are warranted or recommended at this intersection.

## Recommendations

Based on the capacity analysis, the following improvements are recommended to accommodate the projected 2020 traffic volumes:

## U.S. 60 at Lightfoot Road / Williamsburg Outlet Mall Driveway:

- Extend the eastbound left-turn lane on U.S. 60 from 275 feet to 325 feet


## Lightfoot Road at Proposed Right-in / Right-out / Left-out Driveway:

- Construct the site driveway with one ingress lane and two egress lanes
- Construct a southbound taper on Lightfoot Road

Figure 13 shows the recommended roadway laneage.

## Ms. Susan Kassel

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Based on the results of the traffic capacity analysis, we recommend approval of the AME request for the existing right-in / right-out driveway on U.S. 60 that will remain for the following reasons:

- The applicant will close the eastern right-in / right-out driveway on U.S. 60
- The full-movement site driveway on Lightfoot Road will be downgraded to a partial access driveway, and shifted approximately 180 feet to the north to increase the separation from U.S. 60
- All of the study intersections will function at an acceptable overall level-of-service at build-out of the proposed redevelopment
- Figure 14 shows that this site is on an established business corridor on a highway where the existing driveway spacing does not meet current standards

We appreciate your attention to this matter. Please contact me at (804) 217-8560 if you have any questions about this report.

Sincerely yours,
Ramey Kemp \& Associates, Inc.

Carl Hultgren, P.E., PTOE
Regional Manager


Enclosures: Figures, VDOT turn lane warrant diagram, Traffic count data, Synchro output
Copy to: Mr. Paul Holt, AICP, York County Planning
Ms. Ellen Cook, York County Planning
Mr. Jason Fowler, P.E., VDOT
Mr. Glenn Brooks, P.E., VDOT
Mr. Andy Sadler, Woodfin
Mr. Timothy Trant, Kaufman \& Canoles, P.C.
Mr. Dan Caskie, P.E., Bay Companies


Overview

|  | Lightfoot Road C-Store <br> York County and James City County, Virginia | Site Location and Study Intersections |  |
| :---: | :---: | :---: | :---: |
|  |  | Scale: Not to Scale | Figure 1 |



| RAMEY KEMP ASSOCIATES <br> TRANSPORTATION ENGINEERS | Lightfoot Road C-Store York County and James City County, Virginia | Conceptual Site Plan |  |
| :---: | :---: | :---: | :---: |
|  |  | Scale: Not to Scale | Figure 2 |




## LEGEND

X (Y) AM (PM) Peak Hour

|  | Lightfoot Road C-Store York County and James City County, Virginia | Existing (2018) <br> Peak Hour Traffic Volumes |  |
| :---: | :---: | :---: | :---: |
|  |  | Scale: Not to Scale | Figure 4 |






## LEGEND

X (Y) AM (PM) Peak Hour

| ORAMEY KEMP | Lightfoot Road C-Store York County and James City County, Virginia | No-Build (2020) Peak Hour Traffic Volumes |  |
| :---: | :---: | :---: | :---: |
|  |  | Scale: Not to Scale | Figure 8 |



## LEGEND

X (Y) AM (PM) Peak Hour

| RAMEY KEMP ASSOCIATES <br> TRANSPORTATION ENGINEERS | Lightfoot Road C-Store <br> York County and James City County, Virginia | Existing Site Trip Adjustment |  |
| :---: | :---: | :---: | :---: |
|  |  | Scale: Not to Scale | Figure 9 |







## LEGEND

X' Intersection Spacing (In Feet)

## RAMEY KEMP ASSOCIATES

Lightfoot Road C-Store
York County and James City County, Virginia

1/31/2007 Aerial of Corridor


Appropriate Radius required at all Intersections and Entrances (Commercial or Private).

## LEGEND

PHV - Peak Hour Volume (also Design Hourly Volume equivalent)

## Adjustment for Right Turns

For posted speeds at or under $45 \mathrm{mph}, \mathrm{PHV}$ right turns $>40$, and PHV total < 300.
Adjusted right turns = PHV Right Turns - 20
If PHV is not known use formula: $\mathrm{PHV}=\mathrm{ADT} \times \mathrm{K} \times \mathrm{D}$
$\mathrm{K}=$ the percent of $A A D T$ occurring in the peak hour
$D=$ the percent of traffic in the peak direction of flow
Note: An average of $11 \%$ for $\mathrm{K} \times \mathrm{D}$ will suffice.
When right turn facilities are warranted, see Figure 3-1 for design criteria.*
FIGURE 3-26 WARRANTS FOR RIGHT TURN TREATMENT (2-LANE HIGHWAY)

# VHB Engineering NC, P.C. 

4000 WestChase Boulevard, Suite 530
Raleigh, NC 27607
p: 919-829-0328 f: 919.833-0034
File Name : US60@Lightfoot
Site Code :
Start Date : 10/20/2016
Page No : 1
Groups Printed- Passenger Vehicles - Single Unit - TTST - Bicycles on Crosswalk - Pedestrians

|  | US 60 (Richmond Road) Southbound |  |  |  | Lightfoot Road Westbound |  |  |  | US 60 (Richmond Road) Northbound |  |  |  | Lightfoot Road Eastbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Exclu. Total | Inclu. Total | Int. Total |
| 07:00 AM | 33 | 151 | 47 | 0 | 35 | 20 | 24 | 0 | 10 | 118 | 21 | 0 | 5 | 1 | 8 | 0 | 0 | 473 | 473 |
| 07:15 AM | 27 | 140 | 13 | 0 | 15 | 9 | 25 | 0 | 11 | 138 | 24 | 0 | 6 | 3 | 8 | 0 | 0 | 419 | 419 |
| 07:30 AM | 35 | 152 | 18 | 0 | 32 | 8 | 33 | 0 | 6 | 81 | 28 | 0 | 7 | 5 | 15 | 0 | 0 | 420 | 420 |
| 07:45 AM | 51 | 160 | 9 | 1 | 24 | 9 | 38 | 0 | 7 | 112 | 31 | 0 | 14 | 7 | 5 | 0 | 1 | 467 | 468 |
| Total | 146 | 603 | 87 | 1 | 106 | 46 | 120 | 0 | 34 | 449 | 104 | 0 | 32 | 16 | 36 | 0 | 1 | 1779 | 1780 |
| 08:00 AM | 40 | 144 | 13 | 0 | 20 | 8 | 25 | 2 | 9 | 109 | 31 | 0 | 9 | 5 | 10 | 0 | 2 | 423 | 425 |
| 08:15 AM | 50 | 132 | 5 | 0 | 25 | 8 | 39 | 0 | 3 | 113 | 38 | 0 | 7 | 4 | 9 | 0 | 0 | 433 | 433 |
| 08:30 AM | 53 | 153 | 16 | 0 | 27 | 10 | 44 | 0 | 5 | 105 | 19 | 0 | 9 | 3 | 8 | 0 | 0 | 452 | 452 |
| 08:45 AM | 49 | 146 | 20 | 0 | 45 | 11 | 45 | 0 | 7 | 140 | 43 | 0 | 11 | 8 | 9 | 0 | 0 | 534 | 534 |
| Total | 192 | 575 | 54 | 0 | 117 | 37 | 153 | 2 | 24 | 467 | 131 | 0 | 36 | 20 | 36 | 0 | 2 | 1842 | 1844 |
| *** BREAK *** |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 04:00 PM | 60 | 216 | 17 | 0 | 51 | 8 | 82 | 0 | 6 | 195 | 47 | 0 | 17 | 8 | 16 | 0 | 0 | 723 | 723 |
| 04:15 PM | 55 | 181 | 27 | 0 | 58 | 8 | 67 | 0 | 14 | 221 | 48 | 0 | 12 | 9 | 10 | 0 | 0 | 710 | 710 |
| 04:30 PM | 68 | 195 | 18 | 0 | 52 | 18 | 80 | 0 | 11 | 210 | 56 | 0 | 20 | 10 | 16 | 0 | 0 | 754 | 754 |
| 04:45 PM | 53 | 201 | 16 | 0 | 67 | 8 | 94 | 0 | 17 | 208 | 40 | 0 | 22 | 10 | 16 | 0 | 0 | 752 | 752 |
| Total | 236 | 793 | 78 | 0 | 228 | 42 | 323 | 0 | 48 | 834 | 191 | 0 | 71 | 37 | 58 | 0 | 0 | 2939 | 2939 |
| 05:00 PM | 54 | 204 | 15 | 0 | 57 | 12 | 68 | 0 | 14 | 201 | 55 | 0 | 17 | 12 | 11 | 0 | 0 | 720 | 720 |
| 05:15 PM | 43 | 248 | 21 | 0 | 67 | 9 | 74 | 0 | 18 | 243 | 50 | 0 | 16 | 7 | 16 | 0 | 0 | 812 | 812 |
| 05:30 PM | 42 | 211 | 22 | 0 | 57 | 10 | 68 | 0 | 10 | 183 | 44 | 0 | 21 | 12 | 10 | 0 | 0 | 690 | 690 |
| 05:45 PM | 51 | 185 | 25 | 0 | 65 | 10 | 61 | 0 | 19 | 173 | 56 | 0 | 16 | 7 | 21 | 0 | 0 | 689 | 689 |
| Total | 190 | 848 | 83 | 0 | 246 | 41 | 271 | 0 | 61 | 800 | 205 | 0 | 70 | 38 | 58 | 0 | 0 | 2911 | 2911 |
| Grand Total | 764 | 2819 | 302 | 1 | 697 | 166 | 867 | 2 | 167 | 2550 | 631 | 0 | 209 | 111 | 188 | 0 | 3 | 9471 | 9474 |
| Apprch \% | 19.7 | 72.6 | 7.8 |  | 40.3 | 9.6 | 50.1 |  | 5 | 76.2 | 18.8 |  | 41.1 | 21.9 | 37 |  |  |  |  |
| Total \% | 8.1 | 29.8 | 3.2 |  | 7.4 | 1.8 | 9.2 |  | 1.8 | 26.9 | 6.7 |  | 2.2 | 1.2 | 2 |  | 0 | 100 |  |
| Passenger Vehicles | 746 | 2735 | 297 |  | 684 | 160 | 851 |  | 166 | 2475 | 622 |  | 201 | 110 | 185 |  | 0 | 0 | 9232 |
| \% Passenger Vehicles | 97.6 | 97 | 98.3 | 0 | 98.1 | 96.4 | 98.2 | 0 | 99.4 | 97.1 | 98.6 | 0 | 96.2 | 99.1 | 98.4 | 0 | 0 | 0 | 97.4 |
| Single Unit | 14 | 81 | 4 |  | 12 | 6 | 15 |  | 0 | 72 | 8 |  | 8 | 0 | 3 |  | 0 | 0 | 223 |
| \% Single Unit | 1.8 | 2.9 | 1.3 | 0 | 1.7 | 3.6 | 1.7 | 0 | 0 | 2.8 | 1.3 | 0 | 3.8 | 0 | 1.6 | 0 | 0 | 0 | 2.4 |
| TTST | 4 | 3 | 1 |  | 1 | 0 | 1 |  | 1 | 3 | 1 |  | 0 | 1 | 0 |  | 0 | 0 | 16 |
| \% TTST | 0.5 | 0.1 | 0.3 | 0 | 0.1 | 0 | 0.1 | 0 | 0.6 | 0.1 | 0.2 | 0 | 0 | 0.9 | 0 | 0 | 0 | 0 | 0.2 |
| Bicycles on Crosswalk | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |
| \% Bicycles on Crosswalk | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pedestrians | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 3 |
| \% Pedestrians | 0 | 0 | 0 | 100 | 0 | 0 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

# Peggy Malone \& Associates <br> (888) 247-8602 

File Name : 1-US 60 and Exxon Driveways AM
Site Code : 00000000
Start Date : 6/12/2018
Page No :1
Groups Printed- All Vehicles (no classification)

|  | US 60 Southbound |  |  |  |  | fake approach Westbound |  |  |  |  | US 60 Northbound |  |  |  |  | Exxon (N) Driveway Southwestbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Thru | Left | Hard Left | Peds | App. Total | Hard <br> Right | Right | Left | Peds | App. Total | Right | $\begin{aligned} & \text { Bear } \\ & \text { Right } \end{aligned}$ | Thru | Peds | App. Total | Hard Righe | Bear Left | Hard Left | Peds | App. Total | Int. Total |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 3 | 3 | 0 | 0 | 0 | 3 | 6 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 3 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 2 | 6 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 3 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 2 | 6 | 0 | 0 | 8 | 7 | 0 | 0 | 0 | 7 | 17 |


| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 3 | 4 | 0 | 0 | 0 | 4 | 7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 4 | 0 | 0 | 7 | 7 | 0 | 0 | 0 | 7 | 14 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 4 | 6 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 3 | 0 | 0 | 0 | 3 | 7 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 12 | 0 | 0 | 16 | 18 | 0 | 0 | 0 | 18 | 34 |



|  | US 60 Southbound |  |  |  |  | fake approach Westbound |  |  |  |  | US 60 Northbound |  |  |  |  | Exxon (N) Driveway Southwestbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Thru | Left | Hard Left | Peds | App. Total | Hard | Right | Left | Peds | App. Total | Right | Bear | Thru | Peds | App. Total | Hard | Bear Left | Hard Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 08:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 3 | 4 | 0 | 0 | 0 | 4 | 7 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 4 | 0 | 0 | 7 | 7 | 0 | 0 | 0 | 7 | 14 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 4 | 6 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 3 | 0 | 0 | 0 | 3 | 7 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 12 | 0 | 0 | 16 | 18 | 0 | 0 | 0 | 18 | 34 |
| \% App. Total | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 25 | 75 | 0 | 0 |  | 100 | 0 | 0 | 0 |  |  |
| PHF | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 333 | . 750 | . 000 | . 000 | . 571 | . 643 | . 000 | . 000 | . 000 | . 643 | . 607 |

# Peggy Malone \& Associates <br> (888) 247-8602 

File Name : 1-US 60 and Exxon Driveways PM
Site Code : 00000000
Start Date : 6/12/2018
Page No : 1
Groups Printed- All Vehicles (no classification)

|  | US 60 Southbound |  |  |  | fake approach Westbound |  |  |  | US 60 Northbound |  |  |  | Exxon (N) Driveway Southwestbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Thru | Left | Hard Left | App. Total | Hard Right | Right | Left | App. Total | Right | Bear Right | Thru | App. Total | Hard Right | Bear Left | Hard Left | App. Total | Int. Total |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 5 | 0 | 5 | 5 | 0 | 0 | 5 | 11 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 3 | 0 | 4 | 8 | 0 | 0 | 8 | 13 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 4 | 5 | 0 | 0 | 5 | 9 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 2 | 0 | 0 | 2 | 3 |
| Total | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 2 | 12 | 0 | 14 | 20 | 0 | 0 | 20 | 36 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 3 | 0 | 3 | 7 | 0 | 0 | 7 | 12 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 6 | 0 | 0 | 6 | 8 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 2 | 0 | 0 | 2 | 4 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 1 | 0 | 1 | 4 | 0 | 0 | 4 | 7 |
| Total | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 8 | 0 | 8 | 19 | 0 | 0 | 19 | 31 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 6 | 2 | 20 | 0 | 22 | 39 | 0 | 0 | 39 | 67 |
| Apprch \% | 0 | 0 | 0 |  | 0 | 100 | 0 |  | 9.1 | 90.9 | 0 |  | 100 | 0 | 0 |  |  |
| Total \% | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 9 | 3 | 29.9 | 0 | 32.8 | 58.2 | 0 | 0 | 58.2 |  |


|  | US 60 Southbound |  |  |  | fake approach Westbound |  |  |  | US 60 Northbound |  |  |  | Exxon (N) Driveway Southwestbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Thru | Left | Hard Left | App. Total | Hard Right | Right | Left | App. Total | Right | Bear Right | Thru | App. Total | Hard Right | Bear Left | Hard Left | App. Total | Int. Total |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 Peak Hour for Entire Intersection Begins at 04:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 3 | 0 | 4 | 8 | 0 | 0 | 8 | 13 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 4 | 5 | 0 | 0 | 5 | 9 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 2 | 0 | 0 | 2 | 3 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 3 | 0 | 3 | 7 | 0 | 0 | 7 | 12 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 2 | 10 | 0 | 12 | 22 | 0 | 0 | 22 | 37 |
| \% App. Total | 0 | 0 | 0 |  | 0 | 100 | 0 |  | 16.7 | 83.3 | 0 |  | 100 | 0 | 0 |  |  |
| PHF | . 000 | . 000 | . 000 | . 000 | . 000 | . 375 | . 000 | . 375 | . 500 | . 833 | . 000 | . 750 | . 688 | . 000 | . 000 | . 688 | . 712 |

# Peggy Malone \& Associates <br> (888) 247-8602 

File Name : 2-Exxon and US 60 AM
Site Code :
Start Date : 6/12/2018
Page No : 1
Groups Printed- All Vehicles (no classification)

|  | Exxon Southbound |  |  |  |  | Lightfoot <br> Westbound |  |  |  | Nissan Northbound |  |  |  |  | Lightfoot Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Left | Peds | App. Total | Int. Total |
| 07:00 AM | 0 | 0 | 3 | 0 | 3 | 4 | 1 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 6 | 14 |
| 07:15 AM | 2 | 0 | 7 | 0 | 9 | 2 | 2 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 4 | 17 |
| 07:30 AM | 2 | 0 | 1 | 0 | 3 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 2 | 1 | 1 | 0 | 2 | 8 |
| 07:45 AM | 1 | 0 | 1 | 0 | 2 | 1 | 3 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 4 | 10 |
| Total | 5 | 0 | 12 | 0 | 17 | 8 | 6 | 0 | 14 | 1 | 0 | 1 | 0 | 2 | 6 | 10 | 0 | 16 | 49 |


| 08:00 AM | 1 | 0 | 1 | 0 | 2 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 3 | 10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 08:15 AM | 0 | 0 | 1 | 1 | 2 | 2 | 1 | 0 | 3 | 1 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 2 | 8 |
| 08:30 AM | 3 | 0 | 4 | 2 | 9 | 3 | 2 | 0 | 5 | 3 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 1 | 18 |
| 08:45 AM | 5 | 0 | 1 | 0 | 6 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 6 | 14 |
| Total | 9 | 0 | 7 | 3 | 19 | 12 | 3 | 0 | 15 | 4 | 0 | 0 | 0 | 4 | 7 | 5 | 0 | 12 | 50 |
| Grand Total | 14 | 0 | 19 | 3 | 36 | 20 | 9 | 0 | 29 | 5 | 0 | 1 | 0 | 6 | 13 | 15 | 0 | 28 | 99 |
| Apprch \% | 38.9 | 0 | 52.8 | 8.3 |  | 69 | 31 | 0 |  | 83.3 | 0 | 16.7 | 0 |  | 46.4 | 53.6 | 0 |  |  |
| Total \% | 14.1 | 0 | 19.2 | 3 | 36.4 | 20.2 | 9.1 | 0 | 29.3 | 5.1 | 0 | 1 | 0 | 6.1 | 13.1 | 15.2 | 0 | 28.3 |  |


|  | Exxon Southbound |  |  |  | Lightfoot <br> Westbound |  |  | Nissan Northbound |  |  |  | Lightfoot Eastbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | App. Total | Right | Left | App. Total | Right | Thru | Left | App. Total | Right | Left | App. Total | Int. Total |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 Peak Hour for Entire Intersection Begins at 07:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 07:00 AM | 0 | $0$ | 3 | 3 | 4 | 1 | 5 | 0 | 0 | 0 | 0 | 1 | 5 | 6 | 14 |
| 07:15 AM | 2 | 0 | 7 | 9 | 2 | 2 | 4 | 0 | 0 | 0 | 0 | 2 | 2 | 4 | 17 |
| 07:30 AM | 2 | 0 | 1 | 3 | 1 | 0 | 1 | 1 | 0 | 1 | 2 | 1 | 1 | 2 | 8 |
| 07:45 AM | 1 | 0 | 1 | 2 | 1 | 3 | 4 | 0 | 0 | 0 | 0 | 2 | 2 | 4 | 10 |
| Total Volume | 5 | 0 | 12 | 17 | 8 | 6 | 14 | 1 | 0 | 1 | 2 | 6 | 10 | 16 | 49 |
| \% App. Total | 29.4 | 0 | 70.6 |  | 57.1 | 42.9 |  | 50 | 0 | 50 |  | 37.5 | 62.5 |  |  |
| PHF | . 625 | . 000 | . 429 | . 472 | . 500 | . 500 | . 700 | . 250 | . 000 | . 250 | . 250 | . 750 | . 500 | . 667 | . 721 |

# Peggy Malone \& Associates <br> (888) 247-8602 

File Name : 2-Exxon and US 60 PM
Site Code :
Start Date : 6/12/2018
Page No : 1
Groups Printed- All Vehicles (no classification)

|  | Exxon Southbound |  |  |  |  | Lightfoot Westbound |  |  |  | Nissan Northbound |  |  |  |  | Lightfoot Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Left | Peds | App. Total | Int. Total |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 4 | 2 | 0 | 6 | 0 | 0 | 5 | 0 | 5 | 1 | 0 | 0 | 1 | 12 |
| 04:15 PM | 1 | 0 | 2 | 0 | 3 | 7 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 13 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | 5 | 2 | 0 | 2 | 0 | 4 | 2 | 1 | 0 | 3 | 12 |
| 04:45 PM | 3 | 0 | 2 | 0 | 5 | 2 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| Total | 4 | 0 | 4 | 0 | 8 | 16 | 5 | 0 | 21 | 2 | 0 | 7 | 0 | 9 | 6 | 1 | 0 | 7 | 45 |


| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 8 | 2 | 0 | 10 | 7 | 1 | 0 | 0 | 8 | 1 | 0 | 0 | 1 | 19 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 05:15 PM | 0 | 1 | 2 | 0 | 3 | 5 | 1 | 0 | 6 | 8 | 1 | 1 | 0 | 10 | 2 | 0 | 0 | 2 | 21 |
| 05:30 PM | 0 | 0 | 2 | 0 | 2 | 5 | 1 | 0 | 6 | 3 | 0 | 4 | 0 | 7 | 1 | 0 | 0 | 1 | 16 |
| 05:45 PM | 2 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 3 | 9 |
| Total | 2 | 1 | 4 | 0 | 7 | 22 | 4 | 0 | 26 | 18 | 2 | 5 | 0 | 25 | 5 | 2 | 0 | 7 | 65 |
| Grand Total | 6 | 1 | 8 | 0 | 15 | 38 | 9 | 0 | 47 | 20 | 2 | 12 | 0 | 34 | 11 | 3 | 0 | 14 | 110 |
| Apprch \% | 40 | 6.7 | 53.3 | 0 |  | 80.9 | 19.1 | 0 |  | 58.8 | 5.9 | 35.3 | 0 |  | 78.6 | 21.4 | 0 |  |  |
| Total \% | 5.5 | 0.9 | 7.3 | 0 | 13.6 | 34.5 | 8.2 | 0 | 42.7 | 18.2 | 1.8 | 10.9 | 0 | 30.9 | 10 | 2.7 | 0 | 12.7 |  |


|  | Exxon <br> Southbound |  |  |  | Lightfoot <br> Westbound |  |  | Nissan Northbound |  |  |  | Lightfoot Eastbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | App. Total | Right | Left | App. Total | Right | Thru | Left | App. Total | Right | Left | App. Total | Int. Total |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 05:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 05:00 PM | 0 | 0 |  | 0 | 8 | 2 | 10 | 7 | 1 | 0 | 8 | 1 | 0 | 1 | 19 |
| 05:15 PM | 0 | 1 | 2 | 3 | 5 | 1 | 6 | 8 | 1 | 1 | 10 | 2 | 0 | 2 | 21 |
| 05:30 PM | 0 | 0 | 2 | 2 | 5 | 1 | 6 | 3 | 0 | 4 | 7 | 1 | 0 | 1 | 16 |
| 05:45 PM | 2 | 0 | 0 | 2 | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 9 |
| Total Volume | 2 | 1 | 4 | 7 | 22 | 4 | 26 | 18 | 2 | 5 | 25 | 5 | 2 | 7 | 65 |
| \% App. Total | 28.6 | 14.3 | 57.1 |  | 84.6 | 15.4 |  | 72 | 8 | 20 |  | 71.4 | 28.6 |  |  |
| PHF | . 250 | . 250 | . 500 | . 583 | . 688 | . 500 | . 650 | . 563 | . 500 | . 313 | . 625 | . 625 | . 250 | . 583 | . 774 |


| Lane Group | \％ | $\rightarrow$ | EBR | WBL | － WBT |  | 4 | ¢ ${ }_{\text {¢ }}$ | $\stackrel{+}{\text { NBR }}$ | SBL | $\stackrel{\downarrow}{\text { ¢ }}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{*}$ | 州 | 「 | ${ }^{7}$ | 坐4 | 「 | ${ }^{7}$ | $\uparrow$ | 「 |  | $\uparrow$ | 7 |
| Traffic Volume（vph） | 196 | 587 | 55 | 24 | 476 | 134 | 37 | 20 | 37 | 119 | 38 | 156 |
| Future Volume（vph） | 196 | 587 | 55 | 24 | 476 | 134 | 37 | 20 | 37 | 119 | 38 | 156 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（t） | 0 |  | 0 | 300 |  | 175 | 0 |  | 100 | 0 |  | 0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 0 |  | 1 |
| Taper Length（t） | 100 |  |  | 100 |  |  | 100 |  |  | 100 |  |  |
| Satd．Flow（prot） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1681 | 1741 | 1583 | 0 | 1794 | 1583 |
| FIt Permitted | 0.950 |  |  | 0.950 |  |  | 0.950 | 0.984 |  |  | 0.963 |  |
| Satd．Flow（perm） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1681 | 1741 | 1583 | 0 | 1794 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 149 |  |  | 208 |  |  | 149 |  |  | 181 |
| Link Speed（mph） |  | 45 |  |  | 45 |  |  | 25 |  |  | 45 |  |
| Link Distance（ t ） |  | 182 |  |  | 666 |  |  | 417 |  |  | 201 |  |
| Travel Time（s） |  | 2.8 |  |  | 10.1 |  |  | 11.4 |  |  | 3.0 |  |
| Peak Hour Factor | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  | 25\％ |  |  |  |  |  |
| Lane Group Flow（vph） | 228 | 683 | 64 | 28 | 553 | 156 | 32 | 34 | 43 | 0 | 182 | 181 |
| Turn Type | Prot | NA | Perm | Prot | NA | Free | Split | NA | Perm | Split | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 3 |  | 4 | 4 |  |
| Permitted Phases |  |  | 2 |  |  | Free |  |  | 3 |  |  | 4 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 3 | 3 | 3 | 4 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 13.0 | 13.0 | 13.0 | 13.0 | 16.0 |  | 16.0 | 16.0 | 16.0 | 16.0 | 16.0 | 16.0 |
| Total Split（s） | 20.0 | 45.0 | 45.0 | 19.0 | 44.0 |  | 20.0 | 20.0 | 20.0 | 26.0 | 26.0 | 26.0 |
| Total Split（\％） | 18．2\％ | 40．9\％ | 40．9\％ | 17．3\％ | 40．0\％ |  | 18．2\％ | 18．2\％ | 18．2\％ | 23．6\％ | 23．6\％ | 23．6\％ |
| Yellow Time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All－Red Time（s） | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 |  | －2．0 | －2．0 | －2．0 |  | －2．0 | －2．0 |
| Total Lost Time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lead | Lead | Lag | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Min | C－Min | None | C－Min |  | None | None | None | None | None | None |
| Act Effct Green（s） | 21.6 | 63.8 | 63.8 | 9.3 | 46.7 | 110.0 | 9.7 | 9.7 | 9.7 |  | 18.3 | 18.3 |
| Actuated g／C Ratio | 0.20 | 0.58 | 0.58 | 0.08 | 0.42 | 1.00 | 0.09 | 0.09 | 0.09 |  | 0.17 | 0.17 |
| v／c Ratio | 0.66 | 0.33 | 0.07 | 0.19 | 0.37 | 0.10 | 0.22 | 0.22 | 0.16 |  | 0.61 | 0.44 |
| Control Delay | 50.1 | 15.8 | 0.1 | 49.1 | 25.1 | 0.1 | 49.4 | 49.4 | 1.2 |  | 50.7 | 8.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |
| Total Delay | 50.1 | 15.8 | 0.1 | 49.1 | 25.1 | 0.1 | 49.4 | 49.4 | 1.2 |  | 50.7 | 8.9 |
| LOS | D | B | A | D | C | A | D | D | A |  | D | A |
| Approach Delay |  | 22.8 |  |  | 20.7 |  |  | 30.4 |  |  | 29.9 |  |
| Approach LOS |  | C |  |  | C |  |  | C |  |  | C |  |
| Queue Length 50th（ft） | 147 | 145 | 0 | 19 | 146 | 0 | 22 | 24 | 0 |  | 120 | 0 |
| Queue Length 95th（ft） | 219 | 218 | 0 | 45 | 207 | 0 | 51 | 53 | 0 |  | 173 | 49 |
| Internal Link Dist（tt） |  | 102 |  |  | 586 |  |  | 337 |  |  | 121 |  |
| Turn Bay Length（ t ） |  |  |  | 300 |  | 175 |  |  | 100 |  |  |  |
| Base Capacity（vph） | 347 | 2051 | 980 | 241 | 1550 | 1583 | 244 | 253 | 357 |  | 365 | 466 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |


| Lane Group | ¢ EBL | $\rightarrow$ | EBR | WBL | - WBT | 4 WBR | 4 | 4 NBT | NBR | ¢ SLL | ¢ SBT | $\stackrel{\downarrow}{\text { ¢ }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Reduced v/c Ratio | 0.66 | 0.33 | 0.07 | 0.12 | 0.36 | 0.10 | 0.13 | 0.13 | 0.12 |  | 0.50 | 0.39 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other

Cycle Length: 110
Actuated Cycle Length: 110
Offset: $0(0 \%)$, Referenced to phase 2:EBT and 6:WBT, Start of Green
Natural Cycle: 65
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.66
Intersection Signal Delay: 23.6
Intersection LOS: C
Intersection Capacity Utilization 49.3\% ICU Level of Service A
Analysis Period (min) 15
Splits and Phases: 1: Commercial Driveway /Lightfoot Road \& U.S. 60


|  |  | Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.3 |  |  |  |  |  |
| Movement E | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | \% | 「 |  | $\uparrow$ | 4 | 「 |
| Traffic Vol, veh/h | 7 |  | 5 | 345 | 304 | 12 |
| Future Vol, veh/h | 7 | 9 | 5 | 345 | 304 | 12 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Stop | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 0 | - | - | - | 50 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | . |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mumt Flow | 8 | 10 | 5 | 375 | 330 | 13 |


| Major/Minor | Minor2 | Major1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Conflicting Flow All | 715 | 330 | 343 | 0 | - |


| Approach | EB | NB | SB |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- | :--- |
| HCM Control Delay, s | 11.9 |  | 0.1 | 0 |  |  |  |
| HCM LOS | B |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBL | NBT EBLn1 EBLn2 | SBT | SBR |  |  |  |
| Capacity (veh/h) | 1216 | - | 395 | 712 | - | - |  |
| HCM Lane V/C Ratio | 0.004 | -0.019 | 0.014 | - | - |  |  |
| HCM Control Delay (s) | 8 | 0 | 14.3 | 10.1 | - | - |  |
| HCM Lane LOS | A | A | B | B | - | - |  |
| HCM 95th \%tile Q(veh) | 0 | - | 0.1 | 0 | - | - |  |


| RKA | Synchro 10 Report |
| :--- | ---: |
| Page 1 |  |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh | 0.1 |  |  |  |  |  |
| Movement E | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 个4 | 个个 | \％ |  | F |
| Traffic Vol，veh／h | 0 | 838 | 653 | 12 | 0 | 18 |
| Future Vol，veh／h | 0 | 838 | 653 | 12 | 0 | 18 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized |  | None | － | None | － | None |
| Storage Length | － | － | － | 0 | － | 0 |
| Veh in Median Storage，\＃ |  | 0 | 0 | － | 0 | － |
| Grade，\％ |  | 0 | 0 | － | 0 | － |
| Peak Hour Factor |  | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles，\％ |  | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 911 | 710 | 13 | 0 | 20 |


| Major／Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | ---: | :--- | :--- | :--- | :--- | :--- |
| Conflicting Flow All | - | 0 | - | 0 | - | 355 |
| $\quad$ Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | - | - | - | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow－up Hdwy | - | - | - | - | - | 3.32 |
| Pot Cap－1 Maneuver | 0 | - | - | - | 0 | 641 |
| $\quad$ Stage 1 | 0 | - | - | - | 0 | - |
| Stage 2 | 0 | - | - | - | 0 | - |
| Platoon blocked，\％ |  | - | - | - |  |  |
| Mov Cap－1 Maneuver | - | - | - | - | - | 641 |
| Mov Cap－2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - |  |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay，S | 0 | 0 | 10.8 |
| HCM LOS |  | $B$ |  |


| Minor Lane／Major Mvmt | EBT | WBT | WBR SBLn1 |
| :--- | :---: | ---: | ---: |
| Capacity（veh／h） | - | - | -641 |
| HCM Lane V／C Ratio | - | - | -0.031 |
| HCM Control Delay（s） | - | - | -10.8 |
| HCM Lane LOS | - | - | - |
| HCM 95th \％tile Q（veh） | - | - | - |
| B | 0.1 |  |  |


| RKA | Synchro 10 Report |
| :--- | ---: |
| Page 2 |  |


| Lane Group | \％ | $\rightarrow$ |  | WBL | － WBT |  | 4 | ¢ ${ }_{\text {¢ }}$ | $\stackrel{+}{\text { NBR }}$ | SBL | $\stackrel{\downarrow}{\dagger}$ | $\stackrel{\downarrow}{\text { SBR }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | 个4 | 「 | ${ }^{*}$ | 个4 | ＂ | ${ }^{*}$ | $\uparrow$ | 「 |  | $\uparrow$ | ${ }^{7}$ |
| Trafic Volume（vph） | 222 | 865 | 71 | 61 | 879 | 205 | 77 | 40 | 60 | 248 | 48 | 322 |
| Future Volume（vph） | 222 | 865 | 71 | 61 | 879 | 205 | 77 | 40 | 60 | 248 | 48 | 322 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（t） | 0 |  | 0 | 300 |  | 175 | 0 |  | 100 | 0 |  | 0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 0 |  | 1 |
| Taper Length（t） | 100 |  |  | 100 |  |  | 100 |  |  | 100 |  |  |
| Satd．Flow（prot） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1681 | 1741 | 1583 | 0 | 1788 | 1583 |
| Flt Permitted | 0.950 |  |  | 0.950 |  |  | 0.950 | 0.984 |  |  | 0.960 |  |
| Satd．Flow（perm） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1681 | 1741 | 1583 | 0 | 1788 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 149 |  |  | 208 |  |  | 149 |  |  | 346 |
| Link Speed（mph） |  | 45 |  |  | 45 |  |  | 25 |  |  | 45 |  |
| Link Distance（t） |  | 182 |  |  | 666 |  |  | 417 |  |  | 201 |  |
| Travel Time（s） |  | 2.8 |  |  | 10.1 |  |  | 11.4 |  |  | 3.0 |  |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  | 25\％ |  |  |  |  |  |
| Lane Group Flow（vph） | 239 | 930 | 76 | 66 | 945 | 220 | 62 | 64 | 65 | 0 | 319 | 346 |
| Turn Type | Prot | NA | Perm | Prot | NA | Free | Split | NA | Perm | Split | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 3 |  | 4 | 4 |  |
| Permitted Phases |  |  | 2 |  |  | Free |  |  | 3 |  |  | 4 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 3 | 3 | 3 | 4 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 13.0 | 13.0 | 13.0 | 13.0 | 16.0 |  | 16.0 | 16.0 | 16.0 | 16.0 | 16.0 | 16.0 |
| Total Split（s） | 20.0 | 45.0 | 45.0 | 19.0 | 44.0 |  | 20.0 | 20.0 | 20.0 | 26.0 | 26.0 | 26.0 |
| Total Split（\％） | 18．2\％ | 40．9\％ | 40．9\％ | 17．3\％ | 40．0\％ |  | 18．2\％ | 18．2\％ | 18．2\％ | 23．6\％ | 23．6\％ | 23．6\％ |
| Yellow Time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All－Red Time（s） | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 |  | －2．0 | －2．0 | －2．0 |  | －2．0 | －2．0 |
| Total Lost Time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lead | Lead | Lag | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Min | C－Min | None | C－Min |  | None | None | None | None | None | None |
| Act Effct Green（s） | 17.7 | 51.6 | 51.6 | 11.4 | 43.0 | 110.0 | 11.4 | 11.4 | 11.4 |  | 24.3 | 24.3 |
| Actuated g／C Ratio | 0.16 | 0.47 | 0.47 | 0.10 | 0.39 | 1.00 | 0.10 | 0.10 | 0.10 |  | 0.22 | 0.22 |
| v／c Ratio | 0.84 | 0.56 | 0.09 | 0.36 | 0.68 | 0.14 | 0.36 | 0.36 | 0.22 |  | 0.81 | 0.56 |
| Control Delay | 71.4 | 25.7 | 0.2 | 50.6 | 32.1 | 0.2 | 50.7 | 50.5 | 1.7 |  | 57.8 | 7.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |
| Total Delay | 71.4 | 25.7 | 0.2 | 50.6 | 32.1 | 0.2 | 50.7 | 50.5 | 1.7 |  | 57.8 | 7.8 |
| LOS | E | C | A | D | C | A | D | D | A |  | E | A |
| Approach Delay |  | 32.9 |  |  | 27.4 |  |  | 33.9 |  |  | 31.8 |  |
| Approach LOS |  | C |  |  | C |  |  | C |  |  | C |  |
| Queue Length 50th（ft） | 169 | 275 | 0 | 44 | 303 | 0 | 43 | 45 | 0 |  | 208 | 0 |
| Queue Length 95th（ft） | \＃320 | 365 | 0 | 85 | 378 | 0 | 85 | 87 | 0 |  | \＃371 | 78 |
| Internal Link Dist（tt） |  | 102 |  |  | 586 |  |  | 337 |  |  | 121 |  |
| Turn Bay Length（ t ） |  |  |  | 300 |  | 175 |  |  | 100 |  |  |  |
| Base Capacity（vph） | 284 | 1660 | 821 | 241 | 1406 | 1583 | 244 | 253 | 357 |  | 397 | 621 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |

1: Commercial Driveway /Lightfoot Road \& U.S. 60
Timing Plan: PM Peak Hour

| Lane Group | ¢ EBL | $\rightarrow$ | EBR | WBL | - WBT | 4 WBR | 4 | 4 NBT | NBR |  | ¢ SBT | $\stackrel{ }{4}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Reduced v/c Ratio | 0.84 | 0.56 | 0.09 | 0.27 | 0.67 | 0.14 | 0.25 | 0.25 | 0.18 |  | 0.80 | 0.56 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other
Cycle Length: 110
Actuated Cycle Length: 110
Offset: 0 ( $0 \%$ ), Referenced to phase 2:EBT and 6:WBT, Start of Green
Natural Cycle: 80
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.84
Intersection Signal Delay: $30.7 \quad$ Intersection LOS: C
Intersection Capacity Utilization 69.5\% ICU Level of Service C
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 1: Commercial Driveway/Lightfoot Road \& U.S. 60


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement E | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | \% | 「 |  | $\uparrow$ | 4 | F |
| Traffic Vol, veh/h | 4 | 3 | 1 | 466 | 615 | 18 |
| Future Vol, veh/h | 4 | 3 | 1 | 466 | 615 | 18 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Stop | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None |  | None |
| Storage Length | 0 | 0 | - | - | - | 50 |
| Veh in Median Storage, \# | \# | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 |  |
| Peak Hour Factor | 92 | 100 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 4 | 3 | 1 | 507 | 668 | 20 |


| Major/Minor | Minor2 | Major1 |  | Major2 |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- | :--- |
| Conflicting Flow All | 11777 | 668 | 688 | 0 | - | 0 |
| $\quad$ Stage 1 | 668 | - | - | - | - | - |
| Stage 2 | 509 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 211 | 458 | 906 | - | - | - |
| $\quad$ Stage 1 | 510 | - | - | - | - | - |
| $\quad$ Stage 2 | 604 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 211 | 458 | 906 | - | - | - |
| Mov Cap-2 Maneuver | 211 | - | - | - | - | - |
| Stage 1 | 509 | - | - | - | - | - |
| Stage 2 | 604 | - | - | - | - | - |


| Approach | EB | NB | SB |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| HCM Control Delay, S | 18.5 |  | 0 | 0 |  |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBL | NBT EBLn1 EBLn2 | SBT | SBR |  |  |
| Capacity (veh/h) | 9006 | - | 211 | 458 | - | - |
| HCM Lane V/C Ratio | 0.001 | -0.021 | 0.007 | - | - |  |
| HCM Control Delay (s) | 9 | 0 | 22.4 | 12.9 | - | - |
| HCM Lane LOS | A | A | C | B | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | 0.1 | 0 | - | - |


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| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 体 | 个. | $\mathbf{F}$ |  | $\mathbf{7}$ |
| Traffic Vol, veh/h | 0 | 1158 | 1270 | 9 | 0 | 20 |
| Future Vol, veh/h | 0 | 1158 | 1270 | 9 | 0 | 20 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | 0 | - | 0 |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 1259 | 1380 | 10 | 0 | 22 |


| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 0 | - | 0 | - | 690 |
| $\quad$ Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | - | - | - | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | - | - | - | - | 3.32 |
| Pot Cap-1 Maneuver | 0 | - | - | - | 0 | 388 |
| Stage 1 | 0 | - | - | - | 0 | - |
| Stage 2 | 0 | - | - | - | 0 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | - | - | - | - | - | 388 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 14.8 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: |
| Capacity (veh/h) | - | - | - |
| 388 |  |  |  |
| HCM Lane V/C Ratio | - | - | -0.056 |
| HCM Control Delay (s) | - | - | - |
| HCM Lane LOS | - | - | - |
| HCM 95th \%tile Q(veh) | - | - | - |


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| Lane Group | FBL | $\rightarrow$ | EBR | WBL | ＊－ |  | 4 | ¢ ${ }_{\text {¢ }}$ | $\stackrel{+}{\text { NBR }}$ | SBL | $\stackrel{\downarrow}{\dagger}$ | $\stackrel{\downarrow}{\text { SBR }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{*}$ | 个个 | $\stackrel{\square}{7}$ | ＊ | 44 | 「 | ＊ | 4 | $\overline{7}$ |  | $\uparrow$ | ${ }^{7}$ |
| Trafic Volume（vph） | 200 | 561 | 128 | 75 | 469 | 144 | 75 | 20 | 88 | 134 | 44 | 179 |
| Future Volume（vph） | 200 | 561 | 128 | 75 | 469 | 144 | 75 | 20 | 88 | 134 | 44 | 179 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（t） | 0 |  | 0 | 300 |  | 175 | 0 |  | 100 | 0 |  | 0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 0 |  | 1 |
| Taper Length（tt） | 100 |  |  | 100 |  |  | 100 |  |  | 100 |  |  |
| Satd．Flow（prot） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1681 | 1720 | 1583 | 0 | 1796 | 1583 |
| Flt Permitted | 0.950 |  |  | 0.950 |  |  | 0.950 | 0.972 |  |  | 0.964 |  |
| Satd．Flow（perm） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1681 | 1720 | 1583 | 0 | 1796 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 149 |  |  | 268 |  |  | 208 |  |  | 208 |
| Link Speed（mph） |  | 45 |  |  | 45 |  |  | 25 |  |  | 45 |  |
| Link Distance（t） |  | 182 |  |  | 666 |  |  | 417 |  |  | 201 |  |
| Travel Time（s） |  | 2.8 |  |  | 10.1 |  |  | 11.4 |  |  | 3.0 |  |
| Peak Hour Factor | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  | 37\％ |  |  |  |  |  |
| Lane Group Flow（vph） | 233 | 652 | 149 | 87 | 545 | 167 | 55 | 55 | 102 | 0 | 207 | 208 |
| Turn Type | Prot | NA | Perm | Prot | NA | Free | Split | NA | Perm | Split | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 3 |  | 4 | 4 |  |
| Permitted Phases |  |  | 2 |  |  | Free |  |  | 3 |  |  | 4 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 3 | 3 | 3 | 4 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 13.0 | 13.0 | 13.0 | 13.0 | 16.0 |  | 16.0 | 16.0 | 16.0 | 16.0 | 16.0 | 16.0 |
| Total Split（s） | 31.0 | 48.0 | 48.0 | 17.0 | 34.0 |  | 17.0 | 17.0 | 17.0 | 28.0 | 28.0 | 28.0 |
| Total Split（\％） | 28．2\％ | 43．6\％ | 43．6\％ | 15．5\％ | 30．9\％ |  | 15．5\％ | 15．5\％ | 15．5\％ | 25．5\％ | 25．5\％ | 25．5\％ |
| Yellow Time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All－Red Time（s） | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 |  | －2．0 | －2．0 | －2．0 |  | －2．0 | －2．0 |
| Total Lost Time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lead | Lead | Lag | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Min | C－Min | None | C－Min |  | None | None | None | None | None | None |
| Act Effct Green（s） | 21.4 | 54.5 | 54.5 | 11.9 | 42.5 | 110.0 | 10.7 | 10.7 | 10.7 |  | 19.4 | 19.4 |
| Actuated g／C Ratio | 0.19 | 0.50 | 0.50 | 0.11 | 0.39 | 1.00 | 0.10 | 0.10 | 0.10 |  | 0.18 | 0.18 |
| v／c Ratio | 0.68 | 0.37 | 0.17 | 0.45 | 0.40 | 0.11 | 0.34 | 0.33 | 0.30 |  | 0.66 | 0.46 |
| Control Delay | 50.8 | 20.3 | 4.0 | 53.4 | 27.9 | 0.1 | 51.3 | 51.0 | 2.2 |  | 51.7 | 8.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |
| Total Delay | 50.8 | 20.3 | 4.0 | 53.4 | 27.9 | 0.1 | 51.3 | 51.0 | 2.2 |  | 51.7 | 8.6 |
| LOS | D | C | A | D | C | A | D | D | A |  | D | A |
| Approach Delay |  | 24.8 |  |  | 24.9 |  |  | 27.6 |  |  | 30.1 |  |
| Approach LOS |  | C |  |  | C |  |  | C |  |  | C |  |
| Queue Length 50th（tt） | 153 | 156 | 0 | 58 | 147 | 0 | 38 | 38 | 0 |  | 137 | 0 |
| Queue Length 95th（ft） | 212 | 214 | 34 | 104 | 218 | 0 | 76 | 76 | 0 |  | 195 | 52 |
| Internal Link Dist（tt） |  | 102 |  |  | 586 |  |  | 337 |  |  | 121 |  |
| Turn Bay Length（ t ） |  |  |  | 300 |  | 175 |  |  | 100 |  |  |  |
| Base Capacity（vph） | 434 | 1752 | 859 | 213 | 1367 | 1583 | 198 | 203 | 370 |  | 391 | 508 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |

1: Commercial Driveway /Lightfoot Road \& U.S. 60
Timing Plan: AM Peak Hour

| Lane Group | ¢ EBL | $\rightarrow$ | EBR | WBL | - WBT | 4 WBR | 4 | 4 NBT | NBR |  | ¢ SBT | $\stackrel{ }{4}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Reduced v/c Ratio | 0.54 | 0.37 | 0.17 | 0.41 | 0.40 | 0.11 | 0.28 | 0.27 | 0.28 |  | 0.53 | 0.41 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other
Cycle Length: 110
Actuated Cycle Length: 110
Offset: 0 ( $0 \%$ ), Referenced to phase 2:EBT and 6:WBT, Start of Green
Natural Cycle: 65
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.68
Intersection Signal Delay: 26.0
Intersection LOS: C
Intersection Capacity Utilization 50.4\% ICU Level of Service A
Analysis Period (min) 15
Splits and Phases: 1: Commercial Driveway/Lightfoot Road \& U.S. 60


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.3 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | $\mathbf{T}$ | $\mathbf{7}$ |  | $\mathbf{4}$ | 4 | $\mathbf{T}$ |
| Traffic Vol, veh/h | 7 | 9 | 5 | 359 | 348 | 12 |
| Future Vol, veh/h | 7 | 9 | 5 | 359 | 348 | 12 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 0 | - | - | - | 50 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 8 | 10 | 5 | 390 | 378 | 13 |


| Major/Minor | Minor2 | Major1 |  |  | Major2 |  |
| :--- | ---: | ---: | ---: | :--- | :--- | :--- |
| Conflicting Flow All | 778 | 378 | 391 | 0 | - | 0 |
| $\quad$ Stage 1 | 378 | - | - | - | - | - |
| Stage 2 | 400 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 365 | 669 | 1168 | - | - | - |
| $\quad$ Stage 1 | 693 | - | - | - | - | - |
| Stage 2 | 677 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 363 | 669 | 1168 | - | - | - |
| Mov Cap-2 Maneuver | 363 | - | - | - | - | - |
| Stage 1 | 690 | - | - | - | - | - |
| Stage 2 | 677 | - | - | - | - | - |


| Approach | EB |  | NB | SB |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- | :---: | :---: | :---: | :---: | :---: |
| HCM Control Delay, s | 12.5 |  | 0.1 |  | 0 |  |  |  |  |  |  |
| HCM LOS | B |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBL | NBT EBLn1 EBLn2 | SBT | SBR |  |  |  |  |  |  |
| Capacity (veh/h) | 1168 | - | 363 | 669 | - | - |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.005 | - | 0.021 | 0.015 | - | - |  |  |  |  |  |
| HCM Control Delay (s) | 8.1 | 0 | 15.1 | 10.5 | - | - |  |  |  |  |  |
| HCM Lane LOS | A | A | C | B | - | - |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | 0 | - | 0.1 | 0 | - | - |  |  |  |  |  |


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| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay，s／veh | 0.1 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 个． | 个． | 「 |  | $\mathbf{F}$ |
| Traffic Vol，veh／h | 0 | 889 | 707 | 12 | 0 | 18 |
| Future Vol，veh／h | 0 | 889 | 707 | 12 | 0 | 18 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | 0 | - | 0 |
| Veh in Median Storage，\＃ | - | 0 | 0 | - | 0 | - |
| Grade，\％ | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 966 | 768 | 13 | 0 | 20 |


| Major／Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 0 | - | 0 | - | 384 |
| $\quad$ Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | - | - | - | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow－up Hdwy | - | - | - | - | - | 3.32 |
| Pot Cap－1 Maneuver | 0 | - | - | - | 0 | 614 |
| Stage 1 | 0 | - | - | - | 0 | - |
| Stage 2 | 0 | - | - | - | 0 | - |
| Platoon blocked，\％ |  | - | - | - |  |  |
| Mov Cap－1 Maneuver | - | - | - | - | - | 614 |
| Mov Cap－2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay，s | 0 | 0 | 11.1 |
| HCM LOS |  |  | B |


| Minor Lane／Major Mvmt | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: |
| Capacity（veh／h） | - | - | - |


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|  | 4 | $\rightarrow$ |  | $\downarrow$ | － | 4 | 4 | $\uparrow$ | $\stackrel{ }{ }$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ＊ | 个4 | 「 | ${ }^{1}$ | 44 | 「 | ${ }^{7}$ | ＊ | 「 |  | $\uparrow$ | 「 |
| Traffic Volume（vph） | 228 | 828 | 176 | 144 | 865 | 233 | 172 | 41 | 151 | 260 | 51 | 339 |
| Future Volume（vph） | 228 | 828 | 176 | 144 | 865 | 233 | 172 | 41 | 151 | 260 | 51 | 339 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（ t ） | 0 |  | 0 | 300 |  | 175 | 0 |  | 100 | 0 |  | 0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 0 |  | 1 |
| Taper Length（tt） | 100 |  |  | 100 |  |  | 100 |  |  | 100 |  |  |
| Satd．Flow（prot） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1681 | 1717 | 1583 | 0 | 1788 | 1583 |
| Flt Permitted | 0.950 |  |  | 0.950 |  |  | 0.950 | 0.970 |  |  | 0.960 |  |
| Satd．Flow（perm） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1681 | 1717 | 1583 | 0 | 1788 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 189 |  |  | 208 |  |  | 162 |  |  | 300 |
| Link Speed（mph） |  | 45 |  |  | 45 |  |  | 25 |  |  | 45 |  |
| Link Distance（t） |  | 182 |  |  | 666 |  |  | 417 |  |  | 201 |  |
| Travel Time（s） |  | 2.8 |  |  | 10.1 |  |  | 11.4 |  |  | 3.0 |  |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  | 39\％ |  |  |  |  |  |
| Lane Group Flow（vph） | 245 | 890 | 189 | 155 | 930 | 251 | 113 | 116 | 162 | 0 | 335 | 365 |
| Turn Type | Prot | NA | Perm | Prot | NA | Free | Split | NA | Perm | Split | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 3 |  | 4 | 4 |  |
| Permitted Phases |  |  | 2 |  |  | Free |  |  | 3 |  |  | 4 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 3 | 3 | 3 | 4 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 13.0 | 13.0 | 13.0 | 13.0 | 16.0 |  | 16.0 | 16.0 | 16.0 | 16.0 | 16.0 | 16.0 |
| Total Split（s） | 21.0 | 43.0 | 43.0 | 20.0 | 42.0 |  | 20.0 | 20.0 | 20.0 | 27.0 | 27.0 | 27.0 |
| Total Split（\％） | 19．1\％ | 39．1\％ | 39．1\％ | 18．2\％ | 38．2\％ |  | 18．2\％ | 18．2\％ | 18．2\％ | 24．5\％ | 24．5\％ | 24．5\％ |
| Yellow Time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All－Red Time（s） | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 |  | －2．0 | －2．0 | －2．0 |  | －2．0 | －2．0 |
| Total Lost Time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lead | Lead | Lag | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Min | C－Min | None | C－Min |  | None | None | None | None | None | None |
| Act Effct Green（s） | 17.5 | 41.7 | 41.7 | 14.8 | 39.0 | 110.0 | 13.8 | 13.8 | 13.8 |  | 23.7 | 23.7 |
| Actuated g／C Ratio | 0.16 | 0.38 | 0.38 | 0.13 | 0.35 | 1.00 | 0.13 | 0.13 | 0.13 |  | 0.22 | 0.22 |
| v／c Ratio | 0.87 | 0.66 | 0.26 | 0.65 | 0.74 | 0.16 | 0.54 | 0.54 | 0.48 |  | 0.87 | 0.63 |
| Control Delay | 75.3 | 32.1 | 4.6 | 58.5 | 35.9 | 0.2 | 54.2 | 54.1 | 11.6 |  | 65.4 | 13.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |
| Total Delay | 75.3 | 32.1 | 4.6 | 58.5 | 35.9 | 0.2 | 54.2 | 54.1 | 11.6 |  | 65.4 | 13.8 |
| LOS | E | C | A | E | D | A | D | D | B |  | E | B |
| Approach Delay |  | 36.1 |  |  | 31.8 |  |  | 36.5 |  |  | 38.5 |  |
| Approach LOS |  | D |  |  | C |  |  | D |  |  | D |  |
| Queue Length 50th（t） | 172 | 282 | 0 | 104 | 304 | 0 | 78 | 81 | 0 |  | 228 | 38 |
| Queue Length 95th（ t ） | \＃319 | 356 | 47 | 174 | 382 | 0 | 140 | 141 | 60 |  | \＃396 | 138 |
| Internal Link Dist（tt） |  | 102 |  |  | 586 |  |  | 337 |  |  | 121 |  |
| Turn Bay Length（tt） |  |  |  | 300 |  | 175 |  |  | 100 |  |  |  |
| Base Capacity（vph） | 281 | 1340 | 717 | 257 | 1265 | 1583 | 244 | 249 | 368 |  | 388 | 579 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |


| Lane Group | ¢ EBL | $\rightarrow$ | EBR | WBL | - WBT | 4 WBR | 4 | 4 NBT | NBR | ¢ SLL | ¢ SBT | $\stackrel{\downarrow}{\text { ¢ }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Reduced v/c Ratio | 0.87 | 0.66 | 0.26 | 0.60 | 0.74 | 0.16 | 0.46 | 0.47 | 0.44 |  | 0.86 | 0.63 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other

Cycle Length: 110
Actuated Cycle Length: 110
Offset: $0(0 \%)$, Referenced to phase 2:EBT and $6: W B T$, Start of Green
Natural Cycle: 80
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.87
Intersection Signal Delay: $35.1 \quad$ Intersection LOS: D
Intersection Capacity Utilization 70.3\% ICU Level of Service C
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 1: Commercial Driveway /Lightfoot Road \& U.S. 60


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | $\mathbf{T}$ | $\mathbf{7}$ |  | $\mathbf{4}$ | $\mathbf{4}$ | $\mathbf{F}$ |
| Traffic Vol, veh/h | 4 | 3 | 1 | 501 | 647 | 18 |
| Future Vol, veh/h | 4 | 3 | 1 | 501 | 647 | 18 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 0 | - | - | - | 50 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 100 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 4 | 3 | 1 | 545 | 703 | 20 |


| Major/Minor | Minor2 | Major1 |  | Major2 |  |  |
| :--- | ---: | ---: | ---: | :--- | :--- | :--- |
| Conflicting Flow All | 1250 | 703 | 723 | 0 | - | 0 |
| $\quad$ Stage 1 | 703 | - | - | - | - | - |
| Stage 2 | 547 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 191 | 438 | 879 | - | - | - |
| $\quad$ Stage 1 | 491 | - | - | - | - | - |
| Stage 2 | 580 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 191 | 438 | 879 | - | - | - |
| Mov Cap-2 Maneuver | 191 | - | - | - | - | - |
| Stage 1 | 490 | - | - | - | - | - |
| Stage 2 | 580 | - | - | - | - | - |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 19.8 | 0 | 0 |
| HCM LOS | C |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 EBLn2 | SBT | SBR |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 879 | - | 191 | 438 | - | - |
| HCM Lane V/C Ratio | 0.001 | - | 0.023 | 0.007 | - | - |
| HCM Control Delay (s) | 9.1 | 0 | 24.3 | 13.3 | - | - |
| HCM Lane LOS | A | A | C | B | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | 0.1 | 0 | - | - |


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| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay，s／veh | 0.1 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 个． | 个． | 「 |  | $\mathbf{F}$ |
| Traffic Vol，veh／h | 0 | 1232 | 1368 | 9 | 0 | 20 |
| Future Vol，veh／h | 0 | 1232 | 1368 | 9 | 0 | 20 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | 0 | - | 0 |
| Veh in Median Storage，\＃ | - | 0 | 0 | - | 0 | - |
| Grade，\％ | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 1339 | 1487 | 10 | 0 | 22 |


| Major／Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 0 | - | 0 | - | 744 |
| $\quad$ Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | - | - | - | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow－up Hdwy | - | - | - | - | - | 3.32 |
| Pot Cap－1 Maneuver | 0 | - | - | - | 0 | 357 |
| Stage 1 | 0 | - | - | - | 0 | - |
| Stage 2 | 0 | - | - | - | 0 | - |
| Platoon blocked，\％ |  | - | - | - |  |  |
| Mov Cap－1 Maneuver | - | - | - | - | - | 357 |
| Mov Cap－2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay，s | 0 | 0 | 15.7 |
| HCM LOS |  |  | C |


| Minor Lane／Major Mvmt | EBT | WBT | WBR SBLn1 |
| :--- | :---: | ---: | ---: |
| Capacity（veh／h） | - | - | - |
| 357 |  |  |  |
| HCM Lane V／C Ratio | - | - | -0.061 |
| HCM Control Delay（s） | - | - | - |
| HCM Lane LOS | - | - | - |
| HCM 95th \％tile Q（veh） | - | - | - |


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|  | 3 | $\Rightarrow$ |  | 7 | 6 | $\leftarrow$ | 4 | 4 | $\uparrow$ | - | $\checkmark$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| Lane Configurations |  | $\star$ | $\uparrow \uparrow$ | 7 | $\uparrow$ | $\uparrow \uparrow$ | 7 | 9 | $\uparrow$ | F' |  | $\uparrow$ |
| Traffic Volume (vph) | 45 | 195 | 535 | 128 | 75 | 478 | 144 | 78 | 20 | 88 | 176 | 47 |
| Future Volume (vph) | 45 | 195 | 535 | 128 | 75 | 478 | 144 | 78 | 20 | 88 | 176 | 47 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (t) |  | 0 |  | 0 | 300 |  | 175 | 0 |  | 100 | 0 |  |
| Storage Lanes |  | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 0 |  |
| Taper Length (ft) |  | 100 |  |  | 100 |  |  | 100 |  |  | 100 |  |
| Satd. Flow (prot) | 0 | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1681 | 1718 | 1583 | 0 | 1792 |
| FIt Permitted |  | 0.950 |  |  | 0.950 |  |  | 0.950 | 0.971 |  |  | 0.962 |
| Satd. Flow (perm) | 0 | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1681 | 1718 | 1583 | 0 | 1792 |
| Right Turn on Red |  |  |  | Yes |  |  | Yes |  |  | Yes |  |  |
| Satd. Flow (RTOR) |  |  |  | 149 |  |  | 268 |  |  | 208 |  |  |
| Link Speed (mph) |  |  | 45 |  |  | 45 |  |  | 25 |  |  | 45 |
| Link Distance (t) |  |  | 321 |  |  | 666 |  |  | 417 |  |  | 402 |
| Travel Time (s) |  |  | 4.9 |  |  | 10.1 |  |  | 11.4 |  |  | 6.1 |
| Peak Hour Factor | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  | 38\% |  |  |  |  |
| Lane Group Flow (vph) | 0 | 279 | 622 | 149 | 87 | 556 | 167 | 56 | 58 | 102 | 0 | 260 |
| Turn Type | Prot | Prot | NA | Perm | Prot | NA | Free | Split | NA | Perm | Split | NA |
| Protected Phases | 5 | 5 | 2 |  | 1 | 6 |  | 3 | 3 |  | 4 | 4 |
| Permitted Phases |  |  |  | 2 |  |  | Free |  |  | 3 |  |  |
| Detector Phase | 5 | 5 | 2 | 2 | 1 | 6 |  | 3 | 3 | 3 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 | 16.0 |  | 16.0 | 16.0 | 16.0 | 16.0 | 16.0 |
| Total Split (s) | 32.0 | 32.0 | 49.0 | 49.0 | 15.0 | 32.0 |  | 16.0 | 16.0 | 16.0 | 30.0 | 30.0 |
| Total Split (\%) | 29.1\% | 29.1\% | 44.5\% | 44.5\% | 13.6\% | 29.1\% |  | 14.5\% | 14.5\% | 14.5\% | 27.3\% | 27.3\% |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |  | -2.0 | -2.0 | -2.0 |  | -2.0 |
| Total Lost Time (s) |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |  | 4.0 |
| Lead/Lag | Lead | Lead | Lag | Lag | Lead | Lag |  | Lead | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | C-Min | C-Min | None | C-Min |  | None | None | None | None | None |
| Act Effct Green (s) |  | 23.7 | 52.9 | 52.9 | 10.9 | 37.6 | 110.0 | 10.5 | 10.5 | 10.5 |  | 22.2 |
| Actuated g/C Ratio |  | 0.22 | 0.48 | 0.48 | 0.10 | 0.34 | 1.00 | 0.10 | 0.10 | 0.10 |  | 0.20 |
| v/c Ratio |  | 0.73 | 0.37 | 0.18 | 0.50 | 0.46 | 0.11 | 0.35 | 0.36 | 0.30 |  | 0.72 |
| Control Delay |  | 51.7 | 20.7 | 3.9 | 57.1 | 32.0 | 0.1 | 52.2 | 52.3 | 2.3 |  | 52.2 |
| Queue Delay |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 |
| Total Delay |  | 51.7 | 20.7 | 3.9 | 57.1 | 32.0 | 0.1 | 52.2 | 52.3 | 2.3 |  | 52.2 |
| LOS |  | D | C | A | E | C | A | D | D | A |  | D |
| Approach Delay |  |  | 26.6 |  |  | 28.1 |  |  | 28.7 |  |  | 32.4 |
| Approach LOS |  |  | C |  |  | C |  |  | C |  |  | C |
| Queue Length 50th (t) |  | 183 | 156 | 0 | 58 | 165 | 0 | 38 | 41 | 0 |  | 171 |
| Queue Length 95th (t) |  | 251 | 201 | 34 | 107 | 229 | 0 | 77 | 81 | 0 |  | 239 |
| Internal Link Dist (t) |  |  | 241 |  |  | 586 |  |  | 337 |  |  | 322 |
| Turn Bay Length (tt) |  |  |  |  | 300 |  | 175 |  |  | 100 |  |  |
| Base Capacity (vph) |  | 450 | 1703 | 839 | 183 | 1210 | 1583 | 183 | 187 | 358 |  | 423 |
| Starvation Cap Reductn |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |

1: Commercial Driveway /Lightfoot Road \& U.S. 60

|  | $\checkmark$ |
| :---: | :---: |
| Lane Group | SBR |
| Lanđ Configurations | 7 |
| Traffic Volume (vph) | 179 |
| Future Volume (vph) | 179 |
| Ideal Flow (vphpl) | 1900 |
| Storage Length (t) | 225 |
| Storage Lanes | 1 |
| Taper Length (tt) |  |
| Satd. Flow (prot) | 1583 |
| Flt Permitted |  |
| Satd. Flow (perm) | 1583 |
| Right Turn on Red | Yes |
| Satd. Flow (RTOR) | 208 |
| Link Speed (mph) |  |
| Link Distance ( t ) |  |
| Travel Time (s) |  |
| Peak Hour Factor | 0.86 |
| Shared Lane Traffic (\%) |  |
| Lane Group Flow (vph) | 208 |
| Turn Type | Perm |
| Protected Phases |  |
| Permitted Phases | 4 |
| Detector Phase | 4 |
| Switch Phase |  |
| Minimum Initial (s) | 5.0 |
| Minimum Split (s) | 16.0 |
| Total Split (s) | 30.0 |
| Total Split (\%) | 27.3\% |
| Yellow Time (s) | 4.0 |
| All-Red Time (s) | 2.0 |
| Lost Time Adjust (s) | -2.0 |
| Total Lost Time (s) | 4.0 |
| Lead/Lag | Lag |
| Lead-Lag Optimize? | Yes |
| Recall Mode | None |
| Act Effct Green (s) | 22.2 |
| Actuated g/C Ratio | 0.20 |
| v/c Ratio | 0.43 |
| Control Delay | 7.7 |
| Queue Delay | 0.0 |
| Total Delay | 7.7 |
| LOS | A |
| Approach Delay |  |
| Approach LOS |  |
| Queue Length 50th (tt) | 0 |
| Queue Length 95th (ft) | 51 |
| Internal Link Dist (tt) |  |
| Turn Bay Length (t) | 225 |
| Base Capacity (vph) | 533 |
| Starvation Cap Reductn | 0 |

1: Commercial Driveway /Lightfoot Road \& U.S. 60
Timing Plan: AM Peak Hour

|  | $\pm$ | 7 |  |  | $t$ | 4 | 4 | 4 | 4 | $\cdots$ | * | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| Spillback Cap Reductn |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |
| Storage Cap Reductn |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |
| Reduced v/c Ratio |  | 0.62 | 0.37 | 0.18 | 0.48 | 0.46 | 0.11 | 0.31 | 0.31 | 0.28 |  | 0.61 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 110
Actuated Cycle Length: 110
Offset: 0 (0\%), Referenced to phase 2:EBT and 6:WBT, Start of Green
Natural Cycle: 65
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.73
Intersection Signal Delay: 28.3
Intersection LOS: C
Intersection Capacity Utilization 55.4\% ICU Level of Service B
Analysis Period (min) 15
Splits and Phases: 1: Commercial Driveway /Lightfoot Road \& U.S. 60


|  |  |  |  |  |
| :--- | ---: | :---: | :---: | :---: |
| Lane Group | SBR |  |  |  |
| Spillback Cap Reductn | 0 |  |  |  |
| Storage Cap Reductn | 0 |  |  |  |
| Reduced v/c Ratio | 0.39 |  |  |  |
| Intersection Summary |  |  |  |  |



| Major/Minor | Minor2 | Major1 |  | Major2 |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- | :--- |
| Conflicting Flow All | 7777 | 387 | - | 0 | - | 0 |
| $\quad$ Stage 1 | 387 | - | - | - | - | - |
| Stage 2 | 390 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | - | - |
| Pot Cap-1 Maneuver | 365 | 661 | 0 | - | - | - |
| $\quad$ Stage 1 | 686 | - | 0 | - | - | - |
| Stage 2 | 684 | - | 0 | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 365 | 661 | - | - | - | - |
| Mov Cap-2 Maneuver | 365 | - | - | - | - | - |
| Stage 1 | 686 | - | - | - | - | - |
| Stage 2 | 684 | - | - | - | - | - |


| Approach | EB | NB | SB |  |
| :---: | :---: | :---: | :---: | :---: |
| HCM Control Delay, s 1 | 11.9 | 0 | 0 |  |
| HCM LOS | B |  |  |  |
| Minor Lane/Major Mvmt |  | NBT EBLn1 EBLn2 | SBT | SBR |
| Capacity (veh/h) |  | - 365661 | - | - |
| HCM Lane V/C Ratio |  | - 0.0480 .141 | - | - |
| HCM Control Delay (s) |  | - 15.411 .3 | - | - |
| HCM Lane LOS |  | - C B | - | - |
| HCM 95th \%tile Q(veh) |  | - 0.10 .5 | - |  |


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| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.4 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 个. | 个. | $\mathbf{J}$ |  | $\mathbf{7}$ |
| Traffic Vol, veh/h | 0 | 903 | 659 | 153 | 0 | 67 |
| Future Vol, veh/h | 0 | 903 | 659 | 153 | 0 | 67 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | 0 | - | 0 |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 982 | 716 | 166 | 0 | 73 |


| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 0 | - | 0 | - | 358 |
| $\quad$ Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | - | - | - | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | - | - | - | - | 3.32 |
| Pot Cap-1 Maneuver | 0 | - | - | - | 0 | 638 |
| Stage 1 | 0 | - | - | - | 0 | - |
| Stage 2 | 0 | - | - | - | 0 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | - | - | - | - | - | 638 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 11.4 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | EBT | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | - | - | - | 638 |
| HCM Lane V/C Ratio | - | - | -0.114 |  |
| HCM Control Delay (s) | - | - | - | 11.4 |
| HCM Lane LOS | - | - | - | B |
| HCM 95th \%tile Q(veh) | - | - | - | 0.4 |

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|  | 3 | * |  | 7 | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | - | $\checkmark$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| Lane Configurations |  | $\stackrel{y}{*}$ | $\uparrow \uparrow$ | 7 | \% | $\uparrow \uparrow$ | 7 | ${ }^{7}$ | $\uparrow$ | 7 |  | 4 |
| Traffic Volume (vph) | 37 | 227 | 805 | 176 | 144 | 874 | 233 | 174 | 41 | 151 | 299 | 53 |
| Future Volume (vph) | 37 | 227 | 805 | 176 | 144 | 874 | 233 | 174 | 41 | 151 | 299 | 53 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (t) |  | 325 |  | 0 | 300 |  | 175 | 0 |  | 100 | 0 |  |
| Storage Lanes |  | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 0 |  |
| Taper Length (ft) |  | 100 |  |  | 100 |  |  | 100 |  |  | 100 |  |
| Satd. Flow (prot) | 0 | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1681 | 1717 | 1583 | 0 | 1786 |
| Flt Permitted |  | 0.950 |  |  | 0.950 |  |  | 0.950 | 0.970 |  |  | 0.959 |
| Satd. Flow (perm) | 0 | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1681 | 1717 | 1583 | 0 | 1786 |
| Right Turn on Red |  |  |  | Yes |  |  | Yes |  |  | Yes |  |  |
| Satd. Flow (RTOR) |  |  |  | 189 |  |  | 208 |  |  | 162 |  |  |
| Link Speed (mph) |  |  | 45 |  |  | 45 |  |  | 25 |  |  | 45 |
| Link Distance (ft) |  |  | 321 |  |  | 666 |  |  | 417 |  |  | 407 |
| Travel Time (s) |  |  | 4.9 |  |  | 10.1 |  |  | 11.4 |  |  | 6.2 |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  | 39\% |  |  |  |  |
| Lane Group Flow (vph) | 0 | 284 | 866 | 189 | 155 | 940 | 251 | 114 | 117 | 162 | 0 | 379 |
| Turn Type | Prot | Prot | NA | Perm | Prot | NA | Free | Split | NA | Perm | Split | NA |
| Protected Phases | 5 | 5 | 2 |  | 1 | 6 |  | 3 | 3 |  | 4 | 4 |
| Permitted Phases |  |  |  | 2 |  |  | Free |  |  | 3 |  |  |
| Detector Phase | 5 | 5 | 2 | 2 | 1 | 6 |  | 3 | 3 | 3 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 | 16.0 |  | 16.0 | 16.0 | 16.0 | 16.0 | 16.0 |
| Total Split (s) | 27.0 | 27.0 | 42.0 | 42.0 | 21.0 | 36.0 |  | 20.0 | 20.0 | 20.0 | 27.0 | 27.0 |
| Total Split (\%) | 24.5\% | 24.5\% | 38.2\% | 38.2\% | 19.1\% | 32.7\% |  | 18.2\% | 18.2\% | 18.2\% | 24.5\% | 24.5\% |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |  | -2.0 | -2.0 | -2.0 |  | -2.0 |
| Total Lost Time (s) |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |  | 4.0 |
| Lead/Lag | Lead | Lead | Lag | Lag | Lead | Lag |  | Lead | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | C-Min | C-Min | None | C-Min |  | None | None | None | None | None |
| Act Effct Green (s) |  | 21.8 | 39.6 | 39.6 | 15.3 | 33.1 | 110.0 | 13.9 | 13.9 | 13.9 |  | 25.2 |
| Actuated g/C Ratio |  | 0.20 | 0.36 | 0.36 | 0.14 | 0.30 | 1.00 | 0.13 | 0.13 | 0.13 |  | 0.23 |
| v/c Ratio |  | 0.81 | 0.68 | 0.27 | 0.63 | 0.88 | 0.16 | 0.54 | 0.54 | 0.48 |  | 0.93 |
| Control Delay |  | 60.6 | 33.5 | 4.7 | 56.2 | 48.0 | 0.2 | 54.4 | 54.3 | 11.6 |  | 72.7 |
| Queue Delay |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 |
| Total Delay |  | 60.6 | 33.5 | 4.7 | 56.2 | 48.0 | 0.2 | 54.4 | 54.3 | 11.6 |  | 72.7 |
| LOS |  | E | C | A | E | D | A | D | D | B |  | E |
| Approach Delay |  |  | 35.2 |  |  | 40.0 |  |  | 36.7 |  |  | 45.1 |
| Approach LOS |  |  | D |  |  | D |  |  | D |  |  | D |
| Queue Length 50th ( t ) |  | 190 | 275 | 0 | 103 | 337 | 0 | 80 | 82 | 0 |  | 266 |
| Queue Length 95th (t) |  | \#315 | 350 | 47 | 172 | \#458 | 0 | 140 | 143 | 60 |  | \#470 |
| Internal Link Dist (ft) |  |  | 241 |  |  | 586 |  |  | 337 |  |  | 327 |
| Turn Bay Length (t) |  | 325 |  |  | 300 |  | 175 |  |  | 100 |  |  |
| Base Capacity (vph) |  | 370 | 1273 | 690 | 273 | 1066 | 1583 | 244 | 249 | 368 |  | 409 |
| Starvation Cap Reductn |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |

1: Commercial Driveway /Lightfoot Road \& U.S. 60

|  | $\downarrow$ |
| :---: | :---: |
| Lane Group | SBR |
| Lanđ Configurations | 「 |
| Traffic Volume (vph) | 339 |
| Future Volume (vph) | 339 |
| Ideal Flow (vphpl) | 1900 |
| Storage Length (tt) | 225 |
| Storage Lanes | 1 |
| Taper Length ( t ) |  |
| Satd. Flow (prot) | 1583 |
| Flt Permitted |  |
| Satd. Flow (perm) | 1583 |
| Right Turn on Red | Yes |
| Satd. Flow (RTOR) | 272 |
| Link Speed (mph) |  |
| Link Distance (t) |  |
| Travel Time (s) |  |
| Peak Hour Factor | 0.93 |
| Shared Lane Traffic (\%) |  |
| Lane Group Flow (vph) | 365 |
| Turn Type | Perm |
| Protected Phases |  |
| Permitted Phases | 4 |
| Detector Phase | 4 |
| Switch Phase |  |
| Minimum Initial (s) | 5.0 |
| Minimum Split (s) | 16.0 |
| Total Split (s) | 27.0 |
| Total Split (\%) | 24.5\% |
| Yellow Time (s) | 4.0 |
| All-Red Time (s) | 2.0 |
| Lost Time Adjust (s) | -2.0 |
| Total Lost Time (s) | 4.0 |
| Lead/Lag | Lag |
| Lead-Lag Optimize? | Yes |
| Recall Mode | None |
| Act Effct Green (s) | 25.2 |
| Actuated g/C Ratio | 0.23 |
| v/c Ratio | 0.64 |
| Control Delay | 16.4 |
| Queue Delay | 0.0 |
| Total Delay | 16.4 |
| LOS | B |
| Approach Delay |  |
| Approach LOS |  |
| Queue Length 50th (tt) | 55 |
| Queue Length 95th (tt) | 163 |
| Internal Link Dist (ft) |  |
| Turn Bay Length (t) | 225 |
| Base Capacity (vph) | 572 |
| Starvation Cap Reductn | 0 |

1: Commercial Driveway /Lightfoot Road \& U.S. 60
Timing Plan: PM Peak Hour

|  | $\pm$ | 7 |  |  | 6 | 4 | 4 | 4 | 4 | + | * | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| Spillback Cap Reductn |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |
| Storage Cap Reductn |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |
| Reduced v/c Ratio |  | 0.77 | 0.68 | 0.27 | 0.57 | 0.88 | 0.16 | 0.47 | 0.47 | 0.44 |  | 0.93 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 110
Actuated Cycle Length: 110
Offset: 97 (88\%), Referenced to phase 2:EBT and 6:WBT, Start of Green
Natural Cycle: 90
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.93
Intersection Signal Delay: 39.0
Intersection LOS: D
Intersection Capacity Utilization 79.0\% ICU Level of Service D
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 1: Commercial Driveway /Lightfoot Road \& U.S. 60


|  |  |  |  |  |
| :--- | ---: | :---: | :---: | :---: |
| Lane Group | SBR |  |  |  |
| Sillback Cap Reductn | 0 |  |  |  |
| Storage Cap Reductn | 0 |  |  |  |
| Reduced v/c Ratio | 0.64 |  |  |  |
| Intersection Summary |  |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | 1 | $\mathbf{l}$ |  | A | $\uparrow$ |  |
| Traffic Vol, veh/h | 12 | 67 | 0 | 501 | 647 | 12 |
| Future Vol, veh/h | 12 | 67 | 0 | 501 | 647 | 12 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 0 | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 100 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 13 | 67 | 0 | 545 | 703 | 13 |


| Major/Minor | Minor2 | Major1 |  | Major2 |  |  |
| :--- | ---: | ---: | ---: | :--- | :--- | :--- |
| Conflicting Flow All | 1255 | 710 | - | 0 | - | 0 |
| $\quad$ Stage 1 | 710 | - | - | - | - | - |
| $\quad$ Stage 2 | 545 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | - | - |
| Pot Cap-1 Maneuver | 189 | 434 | 0 | - | - | - |
| Stage 1 | 487 | - | 0 | - | - | - |
| Stage 2 | 581 | - | 0 | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 189 | 434 | - | - | - | - |
| Mov Cap-2 Maneuver | 189 | - | - | - | - | - |
| Stage 1 | 487 | - | - | - | - | - |
| Stage 2 | 581 | - | - | - | - | - |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 16.5 | 0 | 0 |
| HCM LOS | C |  |  |


| Minor Lane/Major Mvmt | NBT EBLn1 EBLn2 | SBT | SBR |  |  |
| :--- | ---: | ---: | ---: | :---: | :---: |
| Capacity (veh/h) | - | 189 | 434 | - | - |
| HCM Lane V/C Ratio | -0.069 | 0.154 | - | - |  |
| HCM Control Delay (s) | - | 25.5 | 14.8 | - | - |
| HCM Lane LOS | - | D | B | - | - |
| HCM 95th \%tile Q(veh) | - | 0.2 | 0.5 | - | - |

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| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.4 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 个. | 个. | $\mathbf{J}$ |  | $\mathbf{F}$ |
| Traffic Vol, veh/h | 0 | 1245 | 1321 | 126 | 0 | 59 |
| Future Vol, veh/h | 0 | 1245 | 1321 | 126 | 0 | 59 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | 0 | - | 0 |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 1353 | 1436 | 137 | 0 | 64 |


| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 0 | - | 0 | - | 718 |
| $\quad$ Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | - | - | - | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | - | - | - | - | 3.32 |
| Pot Cap-1 Maneuver | 0 | - | - | - | 0 | 371 |
| $\quad$ Stage 1 | 0 | - | - | - | 0 | - |
| Stage 2 | 0 | - | - | - | 0 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | - | - | - | - | - | 371 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 16.7 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | EBT | WBT | WBR SBLn1 |  |
| :--- | :---: | ---: | ---: | ---: |
| Capacity (veh/h) | - | - | - | 371 |
| HCM Lane V/C Ratio | - | - | -0.173 |  |
| HCM Control Delay (s) | - | - | - | 16.7 |
| HCM Lane LOS | - | - | - | C |
| HCM 95th \%tile Q(veh) | - | - | - | 0.6 |


| RKA | Synchro 10 Report |
| :--- | :--- |

